# TRANSPORTATION ANALYSIS 

## HILLSBOROUGH/ROME DEVELOPMENT

Prepared For

## GILBANE DEVELOPMENT COMPANY

Prepared By


# HILLSBOROUGH/ROME DEVELOPMENT 

Prepared For
GILBANE DEVELOPMENT COMPANY

Prepared By
LINCKS \& ASSOCIATES, INC. 5023 West Laurel Street
Tampa, Florida 33607
813-289-0039
State of Florida Authorization No. EB0004638

November, 2023

Project No. 23145


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## INTRODUCTION

The purpose of this report is to provide a Transportation Analysis in conjunction with the rezoning of the property located south of Hillsborough Avenue and east of Rome Avenue in the City of Tampa, Florida, as shown in Figure 1.

The property currently contains the approximate 38,328 square foot Crosswind Church. In conjunction with the development of the property the existing Church Facilities are to be razed and the new Church building is proposed to be built on the southern portion of the property. With the redevelopment, the property is proposed to be developed for the following land uses:

- Multi-Family - 270 Dwelling Units
- Retail - 2,500 Square Feet
- Relocated Church - 16,000 Square Feet

This analysis was conducted in conformance with the approved Traffic Methodology Statement dated October 23, 2023. A copy of the Traffic Methodology Statement is included in the Appendix of this report.

## ESTIMATED PROJECT AVERAGE DAILY TRAFFIC

The trip rates utilized in this report were obtained from the latest computerized version of "OTISS" which utilizes the Institute of Transportation Engineers' (ITE) Trip Generation Manual, $11^{\text {th }}$ Edition, 2021, as its data base. Table 1 provides the trip generation for the


FIGURE 1
PROJECT LOCATION

(1) Source: ITE Trip Generation Manual, $11^{\text {th }}$ Edition, 2021.
existing and proposed land uses. Based on these trip rates, the net increase in traffic due to the proposed land uses would be approximately 1,193 daily trip ends.

## PROJECT PEAK HOUR TRAFFIC

Again, based on the ITE Trip Generation Manual, $11^{\text {th }}$ Edition, the proposed land uses would result in a net increase of approximately 106 trip ends during the AM peak hour with 25 inbound and 81 outbound, as shown in Table 1.

During the PM peak hour, the proposed land uses would result in a net increase of approximately 124 trip ends with 76 inbound and 48 outbound, as shown in Table 1.

## PROJECT TRIP DISTRIBUTION

The distribution of the project traffic was estimated based on existing traffic and development in the vicinity of the project. Figure 2 illustrates the assignment of the AM and PM peak hour project trip ends on the adjacent transportation network.

## ADJACENT ROADWAYS

As stated previously, the project is located south of Hillsborough Avenue and east of Rome Avenue in the City of Tampa, Florida. Hillsborough Avenue is a four (4) lane divided roadway and Rome Avenue is a two (2) lane undivided roadway in the vicinity of the project.


According to the City of Tampa, Hillsborough County and FDOT Capital Improvement Programs, there are no other capacity adding improvements budgeted in the vicinity of the project.

## STUDY AREA

Based on the Traffic Methodology Statement dated October 23, 2023 included in the Appendix of this report, the study network includes the following intersections:

- Hillsborough Avenue and Armenia Avenue
- Hillsborough Avenue and Rome Avenue
- Hillsborough Avenue and Lee Place


## BUILDOUT

Buildout of the project is anticipated to be 2026.

## BACKGROUND TRAFFIC

The 2026 background traffic utilized in this analysis was calculated as follows:

1) $\mathrm{AM}(7: 00$ to $9: 00)$ peak hour and $\mathrm{PM}(4: 00$ to $6: 00)$ peak hour turning movement counts were conducted at the intersections within the study network, which are as follows:

- Hillsborough Avenue and Armenia Avenue
- Hillsborough Avenue and Rome Avenue
- Hillsborough Avenue and Lee Place

Figure 3 illustrates the existing traffic.
2) The existing counts were adjusted to the peak season based on the FDOT Peak Season Adjustment Factors for Hillsborough County.

Figure 4 illustrates the peak season traffic.
3) The peak season traffic was increased by an annual growth rate of $2.5 \%$ per year to the buildout year of 2026.

Figure 5 illustrates the 2026 background traffic and Figure 6 illustrates the 2026 background plus project traffic for the AM and PM peak hours.

## INTERSECTION ANALYSIS

A capacity analysis was conducted for the AM and PM peak hours at the following intersections:

- Hillsborough Avenue and Armenia Avenue
- Hillsborough Avenue and Rome Avenue
- Hillsborough Avenue and Lee Place

These calculations were performed utilizing the SYNCHRO software. Tables 2 and 3 summarize the results of the analysis and are described in the following paragraphs:



FIGURE 4


FIGURE 5


FIGURE 6
TABLE 2

| AM Peak Hour Background Traffic Existing Geometry |  | RequiredImprovements | AM Peak Hour Background Traffic With Improvements |  | AM Peak Hour Background Plus Project Traffic <br> Background Improvements |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Delay | LOS |  | Delay | LOS | Delay | LOS |
| 74.3 | E | EBR, WBR Signal Timings Modification | 64.6 | E | 64.9 | E |
| 46.9 | D | NBL <br> Signal Timings Modification | 49.1 | D | 50.8 | D |
| 5.1 | A | NBL <br> Signal Timings Modification | 5.2 | A | 5.2 | A |

TABLE 3
 LEVEL OF SERVICE (SIGNALIZED)



-
ゅ $<$
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Hillsborough Ave and

Hillsborough Ave and
Lee Place

## Hillsborough Avenue and Armenia Avenue

Based on signalized intersection analysis, the intersection may operate at a Level of Service E and D during the AM and PM peak hours, respectively, with the 2026 background traffic and existing geometry, as shown in Tables 2 and 3. In an attempt to achieve the adopted level of service within the intersection, an eastbound right turn lane, a westbound right turn lane and minor signal modifications are recommended. With the addition of the project traffic, the intersection should continue to operate at Level of Service E and D during AM and PM peak hours, respectively. It should be noted that the $\mathrm{V} / \mathrm{C}$ ratio for all movements are less than 1.0.

## Hillsborough Avenue and Rome Avenue

Based on signalized intersection analysis, the intersection should operate at a Level of Service D and B during both AM and PM peak hours, with the 2026 background traffic and existing geometry, as shown in Tables 2 and 3. In an attempt to achieve the adopted level of service within the intersection, an northbound left turn lane and minor signal modifications are recommended. With the addition of the project traffic, the intersection should operate at Level of Service $D$ and $C$ during the $A M$ and PM peak hours, respectively. It should be noted that the V/C ratio for all movements are less than 1.0.

## Hillsborough Avenue and Lee Place

Based on signalized intersection analysis, the intersection should operate at a Level of Service A during both AM and PM peak hours, with the 2026 background traffic and existing geometry, as shown in Tables 2 and 3. In an attempt to achieve the adopted Level of Service for all movements, a northbound left turn lane and minor signal modifications
are recommended. With the addition of the project traffic, the intersection should operate at Level of Service A during both AM and PM peak hours. It should be noted that the V/C ratio for all movements are less than 1.0.

## PROPORTIONATE SHARE

As identified in the previous section, improvements are required at the following intersections:

- Hillsborough Avenue and Armenia Avenue
- Hillsborough Avenue and Rome Avenue
- Hillsborough Avenue and Lee Place

Therefore, the following methodology was utilized to determine the project's proportionate share cost of the required improvements identified in the previous section of this report.

1. The following formula was utilized to determine the proportionate share of the required improvements.

Proportionate Share $=($ New Project Traffic/LOS D Capacity $) \times($ Roadway Cost $)$
2. The latest FDOT roadway cost data was utilized for the required improvements.
3. The right-of-way cost was determined to be $125 \%$ of the cost for improvements.

Table 4 summarizes the proportionate share cost for this project which totals $\$ 78,987$.

$$
\text { TABLE } 4
$$



[^0]
## APPENDIX

October 23, 2023

## Ms. Melanie Calloway

City of Tampa
1400 North Boulevard
Tampa, FL 33607
Re: Hillsborough / Rome Development
Lincks Project No. 23145
Dear Ms. Calloway,
The purpose of this letter is to establish the methodology to be utilized for the Transportation Analysis for the proposed development located south of Hillsborough Avenue and east of Rome Avenue in the City of Tampa, Florida, as shown in Figure 1.

The property currently contains the approximate 38,328 square foot Crosswind Church. The property is proposed to be rezoned to allow the following land uses:

- Multi-Family - 270 Dwelling Units
- Retail - 2,500 Square Feet
- Relocated Church - 16,000 Square Feet


## Trip Generation

The trip rates to be utilized in the analysis will be obtained from the latest computerized version of "OTISS" which utilizes the Institute of Transportation Engineers' (ITE) Trip Generation Manual, 11 ${ }^{\text {th }}$ Edition, 2021, as its data base. Table 1 provides the trip generation for the existing and proposed land uses.

## Distribution

The distribution will be based on the existing development patterns in the vicinity of the project.

## Study Network

The study network is proposed to include the following intersections:

- Hillsborough Avenue and Armenia Avenue
- Hillsborough Avenue and Rome Avenue
- Hillsborough Avenue and Lee Place

Ms. Melanie Calloway
October 23, 2023
Page 2


FIGURE 1

Ms. Melanie Calloway
October 23, 2023
Page 3
(1) Source: TTE Trip Generation Manual, $11^{\text {th }}$ Edition, 2021.

## Ms. Melanie Calloway

October 23, 2023
Page 4

## Buildout

Buildout of the project is anticipated to be 2026.

## Background Traffic

The 2026 background traffic to be utilized in this analysis will be calculated as follows:

1) Lincks \& Associates, Inc. will conduct AM (7:00 to 9:00) and PM (4:00 to 6:00) peak hour turning movement counts at the intersections within the study network. The intersections to be included are as follows:

- Hillsborough Avenue and Armenia Avenue
- Hillsborough Avenue and Rome Avenue
- Hillsborough Avenue and Lee Place

2) The existing counts will be adjusted to the peak season based on the 2022 FDOT Peak Season Adjustment Factors for Hillsborough County.
3) The peak season traffic will be increased by an annual growth rate of 2.5\% per year to the buildout year of 2026.

## Signal Timings

The existing signal timings will be utilized for the intersection analysis.

## Analysis Scenario

Intersection capacity analysis shall be conducted based on the SYNCHRO program for Signalized intersections and HCS for Unsignalized intersections.

1) 2026 background plus project traffic with budgeted geometry and signal timings. If the intersection and all movements within the intersection operate at or above the adopted level of service, then no additional analysis is required.
2) 2026 background plus project traffic with the improvements required to allow all movements within the intersection to operate at the adopted level of service.

## Proportionate Share

The proportionate share for any improvements will be determined.

Ms. Melanie Calloway
October 23, 2023
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Please indicate your acceptance of the proposed methodology for the project by signing on the line provided below.


I concur:

Melanie Calloway Date

Enclosures

## APPENDIX



# Bob Henriquez Hillsborough County Property Appraiser 

https://www.hcpafl.org/
15th Floor County Ctr.
601 E. Kennedy Blvd, Tampa, Florida 33602-4932
Ph: (813) 272-6100

## Folio: 105630-0000



## Owner Information

## Owner Name

BETHEL TEMPLE ASSEMBLY OF GOD INC
Mailing Address
Site Address
PIN
Folio
Prior PIN
Prior Folio
Tax District
Property Use
Plat Book/Page
Neighborhood
Subdivision

1510 W HILLSBOROUGH AVE
TAMPA, FL 33603-1208
1510 W HILLSBOROUGH AVE, TAMPA
A-02-29-18-3HF-000019-A0000.0
105630-0000
000000-0000
TA - TAMPA
7100 CHURCHES
29/32
206002.00 | Wellswood Area

3HF | WELLSWOOD SECTION C

| Value Summary |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- |
| Taxing District | Market Value | Assessed Value | Exemptions | Taxable Value |
| County | $\$ 6,022,907$ | $\$ 4,852,174$ | $\$ 4,052,174$ | $\$ 0$ |
| Public Schools | $\$ 6,022,907$ | $\$ 6,022,907$ | $\$ 6,022,907$ | $\$ 0$ |
| Municipal | $\$ 6,022,907$ | $\$ 4,852,174$ | $\$ 4,852,174$ | $\$ 0$ |
| Other Districts | $\$ 6,022,907$ | $\$ 4,852,174$ | $\$ 4,852,174$ | $\$ 0$ |

Note: This section shows Market Value, Assessed Value, Exemptions, and Taxable Value for taxing districts. Because of changes in Florida Law, it is possible to have different assessed and taxable values on the same property. For example, the additional $\$ 25,000$ Homestead Exemption and the non-homestead CAP do not apply to public schools, and the Low Income Senior Exemption only applies to countywide and certain municipal millages.

| Sales Information |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Book / Page | Instrument | Month | Year | Type Inst | Qualified or Unqualified | Vacant or Improved | Price |
| 10050 / 0406 | 2000041949 | 02 | 2000 | WD | Unqualified | Improved | \$205,000 |
| 9611/1828 | 99133710 | 04 | 1999 | WD | Qualified | Improved | \$205,000 |
| 5318 / 0971 | 88013209 | 01 | 1988 | AD | Unqualified | Improved | \$100 |
| 4170 / 0270 |  | 08 | 1983 | WD | Unqualified | Improved | \$90,000 |
| 3280 / 0109 |  | 09 | 1977 |  | Qualified | Improved | \$70,000 |
| 2931/0342 |  | 01 | 1974 |  | Qualified |  | \$20,800 |
| 2635 / 0064 |  | 01 | 1973 |  | Qualified |  | \$22,500 |
| 2564/0665 |  | 01 | 1972 |  | Qualified |  | \$18,500 |
| 2329/0321 |  | 01 | 1971 |  | Qualified |  | \$14,000 |
| 2125/0735 |  | 01 | 1970 |  | Qualified |  | \$0 |



| Building 3 subarea |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Area Type | Gross Area |  | Heated Area |  |  | Depreciated Value |  |
| BAS | 4,204 |  | 4,204 |  |  | \$136,336 |  |
| CAN | 957 |  | 4,204 |  |  | \$9,307 |  |
| Totals |  |  |  |  |  | \$145,643 |  |
| Extra Features |  |  |  |  |  |  |  |
| OB/XF Code coster |  | Building | Year On Roll | Length | Width | Units | Value |
| 0060 CONCRETE PAVEMENT |  | 1 | 1978 | 0 | 0 | 4,020.00 | \$9,535 |
| 0020 ASPHALT PAVING |  | 1 | 2002 | 0 | 0 | 83,300.00 | \$139,944 |
| 0270 FENCE CL8 | , | 0 | 2005 | 0 | 0 | 548.00 | \$6,795 |
| Land Information |  |  |  |  |  |  |  |
| Use Code Description | Zone | Front | Depth | Land Type |  | Total Land Units | Land Value |
| TLHQ TLClass 8 | CG | 0.0 | 0.0 | SF\|SQUA | RE FEET | 43,560.00 | \$598,950 |
| TF3C Hillsborough 7 | CG | 0.0 | 0.0 | SF\|SQUA | RE FEET | 131,685.00 | \$1,501,209 |
| Legal Description |  |  |  |  |  |  |  |

Kimley»）Horn


ITE - TRIP GENERATION MANUAL, $11^{\text {TH }}$ EDITION

## PERIOD SETTING

| Analysis Name : | New Analysis |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Project Name : | Hillsborough - Rome Existing |  | No: |  |  |  |  |
| Date: | 10/20/2023 |  | City: |  |  |  |  |
| State/Province: |  |  | Zip/Postal Code: |  |  |  |  |
| Country: |  |  | Client Name: |  |  |  |  |
| Analyst's Name: |  |  | Edition: |  | Trip Gene Ed | ation M | nual, 11th |
| Land Use | Independent Variable | Size | Time Period | Method | Entry | Exit | Total |
| 560 - Church (General Urban/Suburban) | 1000 Sq. Ft. GFA | 38.33 | Weekday | Average 7.6 | $\begin{aligned} & 146^{(0)} \\ & 50 \% \end{aligned}$ | $\begin{aligned} & 145^{(0)} \\ & 50 \% \end{aligned}$ | $291{ }^{(0)}$ |
| (0) indicates small sam | e size, use carefuly |  |  |  |  |  |  |

## TRAFFIC REDUCTIONS

Land Use
560 - Church

Entry Reduction
$0 \%$

Adjusted Entry
146

Exit Reduction
Adjusted Exit
145

## EXTERNAL TRIPS

| Land Use | External Trips | Pass-by\% | Pass-by Trips | Non-pass-by <br> Trips |
| :--- | :---: | :---: | :---: | :---: |
| $560-$ Church | 291 | 0 | 0 | 291 |

Weekday
Landuse No deviations from ITE.

Methods No deviations from ITE.
External Trips 560 - Church (General Urban/Suburban)
ITE does not recommend a particular pass-by\% for this case.
Total Entering ..... 146
Total Exiting ..... 145
Total Entering Reduction ..... 0
Total Exiting Reduction ..... 0
Total Entering Internal Capture Reduction ..... 0
Total Exiting Internal Capture Reduction ..... 0
Total Entering Pass-by Reduction ..... 0
Total Exiting Pass-by Reduction ..... 0
Total Entering Non-Pass-by Trips ..... 146
Total Exiting Non-Pass-by Trips ..... 145

## PERIOD SETTING



| Land Use | Entry <br> Reduction | Adjusted Entry | Exit Reduction | Adjusted Exit |
| :--- | :--- | :--- | :--- | :--- |
| $560-$ Church | $0 \%$ | 7 | $0 \%$ | 5 |


| Land Use | External Trips | Pass-by\% | Pass-by Trips | Non-pass-by <br> Trips |
| :--- | :---: | :---: | :---: | :---: |
| 560 - Church | 12 | 0 | 0 | 12 |

## ITE DEVIATION DETAILS

Weekday, Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m.
Landuse No deviations from ITE.

Methods No deviations from ITE.

## SUMMARY

Total Entering ..... 7
Total Exiting ..... 5
Total Entering Reduction ..... 0
Total Exiting Reduction ..... 0
Total Entering Internal Capture Reduction ..... 0
Total Exiting Internal Capture Reduction ..... 0
Total Entering Pass-by Reduction ..... 0
Total Exiting Pass-by Reduction ..... 0
Total Entering Non-Pass-by Trips ..... 7
Total Exiting Non-Pass-by Trips ..... 5

## PERIOD SETTING



| TRAFFIC REDUCTIONS |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Land Use | Entry Reduction | Adjusted Entry | Exit Reduction | Adjusted Exit |
| 560 - Church | 0 \% | 8 | $0 \%$ | 11 |
| EXTERNAL TRIPS |  |  |  |  |
| Land Use | External Trips | Pass-by\% | Pass-by Trips | Non-pass-by Trips |
| 560 - Church | 19 | 0 | 0 | 19 |
| ITE DEVIATION DETAILS |  |  |  |  |

Weekday, Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m.

| Landuse |
| :--- |
| No deviations from ITE. |
| Methods |$\quad$ No deviations from ITE.

## SUMMARY

Total Entering ..... 8
Total Exiting ..... 11
Total Entering Reduction ..... 0
Total Exiting Reduction ..... 0
Total Entering Internal Capture Reduction ..... 0
Total Exiting Internal Capture Reduction ..... 0
Total Entering Pass-by Reduction ..... 0
Total Exiting Pass-by Reduction ..... 0
Total Entering Non-Pass-by Trips ..... 8
Total Exiting Non-Pass-by Trips ..... 11

## PERIOD SETTING

| Analysis Name : | New Analysis |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Project Name: | Hillsborough - Rome Proposed |  | No: |  |  |  |  |
| Date: | 10/20/2023 |  | City: |  |  |  |  |
| State/Province: | Zip/Postal Code: |  |  |  |  |  |  |
| Country: | Client Name: |  |  |  |  |  |  |
| Analyst's Name: | Edition: |  |  |  | Trip Gene Ed | ation | ual, 11th |
| Land Use | Independent Variable | Size | Time Period | Method | Entry | Exit | Total |
| 221 - Multifamily Housing (Mid-Rise) Not Close to Rail Transit (General Urban/Suburban) | Dwelling Units | 270 | Weekday | Average 4.54 | $\begin{aligned} & 613 \\ & 50 \% \end{aligned}$ | $\begin{aligned} & 613 \\ & 50 \% \end{aligned}$ | 1226 |
| 822 - Strip Retail <br> Plaza (\<40k) <br> (General <br> Urban/Suburban) | 1000 Sq. Ft. GLA | $2.5{ }^{(0)}$ | Weekday | Average 54.45 | $\begin{aligned} & 688^{(1)} \\ & 50 \% \end{aligned}$ | $\begin{aligned} & 68(1) \\ & 50 \% \end{aligned}$ | $136^{(1)}$ |
| 560 - Church (General Urban/Suburban) | 1000 Sq. Ft. GFA | 16 | Weekday | Average $7.6$ | $\begin{aligned} & 61^{(1)} \\ & 50 \% \end{aligned}$ | $\begin{aligned} & 61(1) \\ & 50 \% \end{aligned}$ | $122^{(1)}$ |
| (0) indicates size out of <br> (1) indicates small sam | range. <br> ple size, use carefuly |  |  |  |  |  |  |

## TRAFFIC REDUCTIONS

| Land Use | Entry <br> Reduction | Adjusted Entry | Exit Reduction | Adjusted Exit |
| :--- | :--- | :--- | :--- | :--- |
| 221 - Multifamily Housing (Mid-Rise) | $0 \%$ | 613 | $0 \%$ | 613 |
| 822 - Strip Retail Plaza (\<40k) | $0 \%$ | 68 | $0 \%$ | 68 |
| 560 - Church | $0 \%$ | 61 | $0 \%$ | 61 |

## INTERNAL TRIPS

## 221 - Multifamily Housing (Mid-Rise)

| Exit | 613 | Demand Exit: |  | (0) | Balanced: 0 | Demand Entry: | $0 \%$ | (0) | Entry 68 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Entry | 613 | Demand Entry: | 0\% | (0) | Balanced: <br> 0 | Demand Exit: | $0 \%$ | (0) | Exit 68 |
| 221 - Multifamily Housing (Mid-Rise) |  |  |  |  |  |  |  |  | 560 - Church |
| Exit | 613 | Demand Exit: | $0 \%$ | (0) | Balanced: 0 | Demand Entry: | $0 \%$ | (0) | Entry 61 |
| Entry | 613 | Demand Entry: | 0\% | (0) | Balanced: | Demand Exit: | 0\% | (0) | Exit $\quad$ '61 |


| Exit | 613 | Demand Exit: | 0 \% | (0) | Balanced: 0 | Demand Entry: | $0 \%$ | (0) | Entry 68 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Entry | 613 | Demand Entry: | $0 \%$ | (0) | Balanced: $0$ | Demand Exit: | $0 \%$ | (0) | Exit 68 |
| 221 - Multifamily Housing (Mid-Rise) |  |  |  |  |  |  |  |  | 560 - Church |
| Exit | 613 | Demand Exit: | $0 \%$ | (0) | Balanced: $0$ | Demand Entry: | $0 \%$ | (0) | Entry 61 |
| Entry | 613 | Demand Entry: | $0 \%$ | (0) | Balanced: | Demand Exit: | 0\% | (0) | Exit 61 |

0 822 - Strip Retail Plaza (8It;40k)

## 822 - Strip Retail Plaza (8It;40k)

560 - Church

| Exit | 68 | Demand Exit: $0 \%$ | $(0)$ |
| :--- | :--- | :--- | :--- | :--- |
| Entry | 68 | Demand Entry: $0 \%$ | $(0)$ |

Balanced:
0
Balanced:
0

Demand Entry: $0 \%$ ( 0
Entry 61
Exit 61

221 - Multifamily Housing (Mid-Rise)

|  | Internal Trips |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | Total Trips | 822 - Strip Retail <br> Plaza (\&ilt;40k) | $\mathbf{5 6 0}$ - Church | Total | External Trips |
| Entry | $613(100 \%)$ | $0(0 \%)$ | $0(0 \%)$ | $0(0 \%)$ | $613(100 \%)$ |
| Exit | $613(100 \%)$ | $0(0 \%)$ | $0(0 \%)$ | $0(0 \%)$ | $613(100 \%)$ |
| Total | $1226(100 \%)$ | $0(0 \%)$ | $0(0 \%)$ | $0(0 \%)$ | $1226(100 \%)$ |

822 - Strip Retail Plaza (\&It;40k)

|  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | Total Trips | Internal Trips |  |  |  |
|  |  | 221 - Multifamily <br> Housing (Mid-Rise) | $\mathbf{5 6 0}$ - Church | Total | External Trips |
| Entry | $68(100 \%)$ | $0(0 \%)$ | $0(0 \%)$ | $0(0 \%)$ | $68(100 \%)$ |
| Exit | $68(100 \%)$ | $0(0 \%)$ | $0(0 \%)$ | $0(0 \%)$ | $68(100 \%)$ |
| Total | $136(100 \%)$ | $0(0 \%)$ | $0(0 \%)$ | $0(0 \%)$ | $136(100 \%)$ |

560 - Church

|  | Total Trips | Internal Trips |  |  | External Trips |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 221 - Multifamily Housing (Mid-Rise) | 822 - Strip Retail Plaza (\&It;40k) | Total |  |
| Entry | 61 (100\%) | 0 (0\%) | 0 (0\%) | 0 (0\%) | 61 (100\%) |
| Exit | 61 (100\%) | 0 (0\%) | 0 (0\%) | 0 (0\%) | 61 (100\%) |
| Total | 122 (100\%) | 0 (0\%) | 0 (0\%) | 0 (0\%) | 122 (100\%) |

## EXTERNAL TRIPS

| Land Use | External Trips | Pass-by\% | Pass-by Trips | Non-pass-by <br> Trips |
| :--- | :---: | :---: | :---: | :---: |
| 221 - Multifamily Housing (Mid-Rise) | 1226 | 0 | 0 | 1226 |
| 822 - Strip Retail Plaza (\<40k) | 136 | 0 | 0 | 136 |
| 560 - Church | 122 | 0 | 0 | 122 |

## Weekday

| Methods | No deviations from ITE. |
| :---: | :---: |
| External Trips | 221 - Multifamily Housing (Mid-Rise) - Not Close to Rail Transit (General Urban/Suburban) ITE does not recommend a particular pass-by\% for this case. |
|  | 822 - Strip Retail Plaza (8lt;40k) (General Urban/Suburban) |
|  | ITE does not recommend a particular pass-by\% for this case. |
|  | 560 - Church (General Urban/Suburban) |
|  | ITE does not recommend a particular pass-by\% for this case. |

## SUMMARY

Total Entering ..... 742
Total Exiting ..... 742
Total Entering Reduction ..... 0
Total Exiting Reduction ..... 0
Total Entering Internal Capture Reduction ..... 0
Total Exiting Internal Capture Reduction ..... 0
Total Entering Pass-by Reduction ..... 0
Total Exiting Pass-by Reduction ..... 0
Total Entering Non-Pass-by Trips ..... 742
Total Exiting Non-Pass-by Trips ..... 742

## PERIOD SETTING

| New Analysis |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Project Name : | Hillsborough - Rome Proposed |  | No: |  |  |  |  |
| Date: | 10/20/2023 |  | City: |  |  |  |  |
| State/Province: |  |  | Zip/Postal Code: |  |  |  |  |
| Country: |  |  | Client Name: |  |  |  |  |
| Analyst's Name: |  |  | Edition: |  | Trip Generation Manual, 11th Ed |  |  |
| Land Use | Independent Variable | Size | Time Period | Method | Entry | Exit | Total |
| 221 - Multifamily Housing (Mid-Rise) Not Close to Rail Transit (General Urban/Suburban) | Dwelling Units | 270 | Weekday, Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m. | Best Fit (LIN) $T=0.44(X)+-11.61$ | $\begin{aligned} & 25 \\ & 23 \% \end{aligned}$ | $\begin{aligned} & 82 \\ & 77 \% \end{aligned}$ | 107 |
| 822 - Strip Retail Plaza (\&It;40k) (General Urban/Suburban) | 1000 Sq. Ft. GLA | $2.5{ }^{(0)}$ | Weekday, Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m. | Average $2.36$ | $\begin{aligned} & 4^{(1)} \\ & 67 \% \end{aligned}$ | $\begin{aligned} & 2^{(1)} \\ & 33 \% \end{aligned}$ | $6^{(1)}$ |
| 560 - Church (General Urban/Suburban) | 1000 Sq. Ft. GFA |  | Weekday, Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m. | Average $0.32$ | $\begin{aligned} & 3 \\ & 60 \% \end{aligned}$ | $\begin{aligned} & 2 \\ & 40 \% \end{aligned}$ | 5 |
| (0) indicates size out of <br> (1) indicates small sam | range. <br> ple size, use carefuly |  |  |  |  |  |  |

## TRAFFIC REDUCTIONS

| Land Use | Entry <br> Reduction | Adjusted Entry | Exit Reduction | Adjusted Exit |
| :--- | :--- | :--- | :--- | :--- |
| 221 - Multifamily Housing (Mid-Rise) | $0 \%$ | 25 | $0 \%$ | 82 |
| 822 - Strip Retail Plaza (\<40k) | $0 \%$ | 4 | $0 \%$ | 2 |
| 560 - Church | $0 \%$ | 3 | $0 \%$ | 2 |

## INTERNAL TRIPS

221 - Multifamily Housing (Mid-Rise)

## 822 - Strip Retail Plaza (8/lt;40k)

Exit 82 Demand Exit: $0 \% \quad(0)$
Balanced:
$0 \quad$ Demand Entry: $0 \%$ ( 0 )
Entry 4

Balanced:
0

Demand Exit: 0 \% (0)
Exit 2

## 221 - Multifamily Housing (Mid-Rise)

Exit $82 \quad$ Demand Exit: $0 \%(0)$
Entry 25 Demand Entry: 0 \% (0)

| Balanced: <br> 0 | Demand Entry: | $0 \%$ | $(0)$ | Entry | 3 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Balanced: <br> 0 | Demand Exit: | $0 \%$ | $(0)$ | Exit | 2 |

## 822 - Strip Retail Plaza (8/t;40k)

| Exit | 2 | Demand Exit: | $0 \%$ | (0) | Balanced: | Demand Entry: $0 \%(0)$ | Entry | 3 |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Entry | 4 | Demand Entry: | $0 \%$ | $(0)$ | Balanced: |  | Demand Exit: | $0 \%$ | $(0)$ |
| Exit | 2 |  |  |  |  |  |  |  |  |


| 221 - Multifamily Housing (Mid-Rise) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total Trips | Internal Trips |  |  | External Trips |
|  |  | 822 - Strip Retail Plaza (8/lt;40k) | 560 - Church | Total |  |
| Entry | 25 (100\%) | 0 (0\%) | 0 (0\%) | 0 (0\%) | 25 (100\%) |
| Exit | 82 (100\%) | 0 (0\%) | 0 (0\%) | 0 (0\%) | 82 (100\%) |
| Total | 107 (100\%) | 0 (0\%) | 0 (0\%) | 0 (0\%) | 107 (100\%) |

822 - Strip Retail Plaza (8/t;40k)

|  | Total Trips | Internal Trips |  |  | External Trips |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 221 - Multifamily Housing (Mid-Rise) | 560 - Church | Total |  |
| Entry | 4 (100\%) | 0 (0\%) | 0 (0\%) | 0 (0\%) | 4 (100\%) |
| Exit | 2 (100\%) | 0 (0\%) | 0 (0\%) | 0 (0\%) | 2 (100\%) |
| Total | 6 (100\%) | 0 (0\%) | 0 (0\%) | 0 (0\%) | 6 (100\%) |

560 - Church

|  |  | Internal Trips |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | Total Trips | 221 - Multifamily <br> Housing (Mid-Rise) | $\mathbf{8 2 2}$ - Strip <br> Retail Plaza <br> (8lt; 40k) | Total | External Trips |
| Entry | $3(100 \%)$ | $0(0 \%)$ | $0(0 \%)$ | $0(0 \%)$ | $3(100 \%)$ |
| Exit | $2(100 \%)$ | $0(0 \%)$ | $0(0 \%)$ | $0(0 \%)$ | $2(100 \%)$ |
| Total | $5(100 \%)$ | $0(0 \%)$ | $0(0 \%)$ | $0(0 \%)$ | $5(100 \%)$ |

## EXTERNAL TRIPS

| Land Use | External Trips | Pass-by\% | Pass-by Trips | Non-pass-by <br> Trips |
| :--- | :---: | :---: | :---: | :---: | :---: |
| 221 - Multifamily Housing (Mid-Rise) | 107 | 0 | 0 | 107 |
| 822 - Strip Retail Plaza (8ilt;40k) | 6 | 0 | 0 | 6 |
| 560 - Church | 5 | 0 | 0 | 5 |

## ITE DEVIATION DETAILS

Weekday, Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m.
Landuse No deviations from ITE.
Methods No deviations from ITE.
External Trips 221 - Multifamily Housing (Mid-Rise) - Not Close to Rail Transit (General Urban/Suburban) ITE does not recommend a particular pass-by\% for this case.

822 - Strip Retail Plaza (\<40k) (General Urban/Suburban)
ITE does not recommend a particular pass-by\% for this case.
560 - Church (General Urban/Suburban)
ITE does not recommend a particular pass-by\% for this case.

## SUMMARY

Total Entering ..... 32
Total Exiting ..... 86
Total Entering Reduction ..... 0
Total Exiting Reduction ..... 0
Total Entering Internal Capture Reduction ..... 0
Total Exiting Internal Capture Reduction ..... 0
Total Entering Pass-by Reduction ..... 0
Total Exiting Pass-by Reduction ..... 0
Total Entering Non-Pass-by Trips ..... 32
Total Exiting Non-Pass-by Trips ..... 86

## PERIOD SETTING

| Analysis Name : | New Analysis |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Project Name: | Hillsborough - Rome Proposed |  | No: |  |  |  |  |
| Date: | 10/20/2023 |  | City: |  |  |  |  |
| State/Province: | Zip/Postal Code: |  |  |  |  |  |  |
| Country: | Client Name: |  |  |  |  |  |  |
| Analyst's Name: |  |  | Edition: |  | Trip Gene Ed | ation | al, 11th |
| Land Use | Independent Variable | Size | Time Period | Method | Entry | Exit | Total |
| 221 - Multifamily Housing (Mid-Rise) Not Close to Rail Transit (General Urban/Suburban) | Dwelling Units | 270 | Weekday, Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m. | Best Fit (LIN) $\mathrm{T}=0.39(\mathrm{X})+0.34$ | $\begin{aligned} & 65 \\ & 61 \% \end{aligned}$ | $\begin{aligned} & 41 \\ & 39 \% \end{aligned}$ | 106 |
| 822 - Strip Retail <br> Plaza (\<40k) <br> (General Urban/Suburban) | 1000 Sq. Ft. GLA |  | Weekday, Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m. | $\begin{aligned} & \text { Best Fit (LOG) } \\ & \operatorname{Ln}(T)=0.71 \operatorname{Ln}(X) \\ & +2.72 \end{aligned}$ | $\begin{aligned} & 15 \\ & 52 \% \end{aligned}$ | $\begin{aligned} & 14 \\ & 48 \% \end{aligned}$ | 29 |
| 560 - Church (General Urban/Suburban) | 1000 Sq. Ft. GFA | 16 | Weekday, Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m. | Average $0.49$ | $\begin{aligned} & 4 \\ & 50 \% \end{aligned}$ | $\begin{aligned} & 4 \\ & 50 \% \end{aligned}$ | 8 |

## TRAFFIC REDUCTIONS

| Land Use | Entry <br> Reduction | Adjusted Entry | Exit Reduction | Adjusted Exit |
| :--- | :--- | :--- | :--- | :--- |
| 221 - Multifamily Housing (Mid-Rise) | $0 \%$ | 65 | $0 \%$ | 41 |
| 822 - Strip Retail Plaza (\&It;40k) | $0 \%$ | 15 | $0 \%$ | 14 |
| 560 - Church | $0 \%$ | 4 | $0 \%$ | 4 |

## INTERNAL TRIPS

221 - Multifamily Housing (Mid-Rise)

| Exit | 41 | Demand Exit: | $0 \%$ | $(0)$ | Balanced: | Demand Entry: $0 \%(0)$ | Entry | 15 |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Entry | 65 | Demand Entry: | $0 \%$ | $(0)$ | Balanced: |  | Demand Exit: | $0 \%$ | $(0)$ |


| Exit | 41 | Demand Exit: | 0 \% | (0) | Balanced: 0 | Demand Entry: | $0 \%$ | (0) | Entry | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Entry | 65 | Demand Entry: | $0 \%$ | (0) | Balanced: 0 | Demand Exit: | 0 \% | (0) | Exit | 4 |
| 822 - | trip | Plaza (8It;40k) |  |  |  |  |  |  | 560 - Churc |  |
| Exit | 14 | Demand Exit: | 0 \% | (0) | Balanced: 0 | Demand Entry: | $0 \%$ | (0) | Entry | 4 |
| Entry | 15 | Demand Entry: | $0 \%$ | (0) | Balanced: 0 | Demand Exit: | 0 \% | (0) | Exit | 4 |

## 221 - Multifamily Housing (Mid-Rise)

|  | Internal Trips <br>  <br>  Total Trips | $\mathbf{8 2 2}$ - Strip Retail <br> Plaza (\&It;40k) | $\mathbf{5 6 0}$ - Church | Total | External Trips |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Entry |  | $0(0 \%)$ | $0(0 \%)$ | $0(0 \%)$ | $65(100 \%)$ |
| Exit |  | $0(0 \%)$ | $0(0 \%)$ | $0(0 \%)$ | $41(100 \%)$ |
| Total | $106(100 \%)$ | $0(0 \%)$ | $0(0 \%)$ | $0(0 \%)$ | $106(100 \%)$ |

822 - Strip Retail Plaza (8.lt;40k)

|  |  |  |  | Internal Trips |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | Total Trips | 221 - Multifamily <br> Housing (Mid-Rise) | $\mathbf{5 6 0}$ - Church | Total | External Trips |
| Entry | $15(100 \%)$ | $0(0 \%)$ | $0(0 \%)$ | $0(0 \%)$ | $15(100 \%)$ |
| Exit | $14(100 \%)$ | $0(0 \%)$ | $0(0 \%)$ | $0(0 \%)$ | $14(100 \%)$ |
| Total | $29(100 \%)$ | $0(0 \%)$ | $0(0 \%)$ | $0(0 \%)$ | $29(100 \%)$ |


| 560 - Church |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total Trips | Internal Trips |  |  | External Trips |
|  |  | 221 - Multifamily Housing (Mid-Rise) | 822 - Strip Retail Plaza (8.lt;40k) | Total |  |
| Entry | 4 (100\%) | 0 (0\%) | 0 (0\%) | 0 (0\%) | 4 (100\%) |
| Exit | 4 (100\%) | 0 (0\%) | 0 (0\%) | 0 (0\%) | 4 (100\%) |
| Total | 8 (100\%) | 0 (0\%) | 0 (0\%) | 0 (0\%) | 8 (100\%) |

## EXTERNAL TRIPS

| Land Use | External Trips | Pass-by\% | Pass-by Trips | Non-pass-by <br> Trips |
| :--- | :---: | :---: | :---: | :---: |
| 221 - Multifamily Housing (Mid-Rise) | 106 | 0 | 0 | 106 |
| 822 - Strip Retail Plaza (\<40k) | 29 | 0 | 0 | 29 |
| 560 - Church | 8 | 0 | 0 | 8 |

Weekday, Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m.
Landuse No deviations from ITE.
Methods No deviations from ITE.
External Trips 221 - Multifamily Housing (Mid-Rise) - Not Close to Rail Transit (General Urban/Suburban) ITE does not recommend a particular pass-by\% for this case.

822 - Strip Retail Plaza (\<40k) (General Urban/Suburban) ITE does not recommend a particular pass-by\% for this case.

560 - Church (General Urban/Suburban)
ITE does not recommend a particular pass-by\% for this case.

## SUMMARY

Total Entering ..... 84
Total Exiting ..... 59
Total Entering Reduction ..... 0
Total Exiting Reduction ..... 0
Total Entering Internal Capture Reduction ..... 0
Total Exiting Internal Capture Reduction ..... 0
Total Entering Pass-by Reduction ..... 0
Total Exiting Pass-by Reduction ..... 0
Total Entering Non-Pass-by Trips ..... 84
Total Exiting Non-Pass-by Trips ..... 59

TURNING MOVEMENT COUNTS


Prepared by National Data \& Surveying Services

## N Armenia Ave \& W Hillsborough Ave/US 92/SR 600

Peak Hour Turning Movement Count

ID: 23-120441-001
City: Tampa

Day: Tuesday
Date: 10/24/2023

National Data \＆Surveying Services

## Intersection Turning Movement Count

Location：N Armenia Ave \＆W Hillsborough Ave／US 92／SR 600
City：Tampa
Control：Signalized

| NS／EW Streets： | Data－Total |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | N Armenia Ave |  |  |  | $N$ Armenia Ave |  |  |  | W Hillsborough Ave／US 92／SR 600 |  |  |  | W Hillsborough Ave／US 92／SR 600 |  |  |  |  |
| AM | NORTHBOUND |  |  |  | SOUTHBOUND |  |  |  | EASTBOUND |  |  |  | WESTBOUND |  |  |  |  |
|  | $0$ | 0 | 0 |  | 0 | 0 | 0 | 0 SU | 0 | $\begin{gathered} 0 \\ \text { FT } \end{gathered}$ | O | 0 FU | $0$ | 0 WT | $0$ WR | $\begin{gathered} 0 \\ \text { WU } \end{gathered}$ |  |
|  | $\mathrm{NL}$ |  | NR | $\mathrm{NU}$ | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 7：00 AM | 22 | 36 | 13 | 0 | 31 | 64 | 13 | 0 | 27 | 372 | 37 | 1 | 11 | 416 | 11 | 1 | 1055 |
| 7：15 AM | 48 | 48 | 22 | 0 | 58 | 122 | 24 | 0 | 42 | 379 | 22 | 0 | 35 | 396 | 12 | 2 | 1210 |
| 7：30 AM | 39 | 62 | 31 | 0 | 70 | 138 | 26 | 0 | 31 | 374 | 48 | 5 | 45 | 462 | 10 | 3 | 1344 |
| 7：45 AM | 39 | 74 | 29 | 0 | 36 | 126 | 17 | 1 | 29 | 389 | 43 | 0 | 49 | 508 | 8 | 5 | 1353 |
| 8：00 AM | 40 | 72 | 15 | 0 | 39 | 138 | 14 | 0 | 37 | 382 | 55 | 2 | 46 | 433 | 17 | 0 | 1290 |
| 8：15 AM | 40 | 71 | 21 | 0 | 35 | 142 | 27 | 0 | 35 | 312 | 38 | 1 | 28 | 422 | 18 | 1 | 1191 |
| 8：30 AM | 32 | 46 | 24 | 0 | 37 | 116 | 21 | 1 | 31 | 357 | 35 | 4 | 36 | 496 | 16 | 2 | 1254 |
| 8：45 AM | 26 | 44 | 13 | 0 | 21 | 121 | 19 | 0 | 25 | 359 | 51 | 4 | 36 | 387 | 18 | 4 | 1128 |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
|  | 286 | 453 | 168 | 0 | 327 | 967 | 161 | 2 | 257 | 2924 | 329 | 17 | 286 | 3520 | 110 | $18$ | 9825 |
| APPROACH \％＇s： | 31．53\％ | 49．94\％ | 18．52\％ | 0．00\％ | 22．44\％ | 66．37\％ | 11．05\％ | 0．14\％ | 7．29\％ | 82．90\％ | 9．33\％ | 0．48\％ | 7．27\％ | 89．48\％ | 2．80\％ | 0．46\％ |  |
| PEAK HR ： | 07：15 AM－08：15 AM |  |  |  | $\begin{gathered} 203 \\ 0.725 \end{gathered}$ | $\begin{aligned} & 524 \\ & 0.949 \\ & 0.80 \end{aligned}$ |  |  | $\begin{aligned} & 139 \\ & 0.827 \end{aligned}$ | $\begin{aligned} & 1524 \\ & 0.979 \end{aligned}$ | $\begin{aligned} & 168 \\ & 0.764 \end{aligned}$ | $\begin{gathered} 7 \\ 0.350 \end{gathered}$ | $\begin{aligned} & 175 \\ & 0.893 \end{aligned}$ | $\begin{aligned} & 1799 \\ & 0.885 \end{aligned}$ | $\begin{gathered} 47 \\ 0.691 \end{gathered}$ | $\begin{gathered} 10 \\ 0.500 \end{gathered}$ | $\begin{aligned} & 5197 \\ & 0.960 \\ & \hline \end{aligned}$ |
| PEAK HR VOL ： | 166 | 256 | 97 | 0 |  |  | 81 | 1 |  |  |  |  |  |  |  |  |  |
| PEAK HR FACTOR ： | 0.865 | 0.865 | 0.782 | 0.000 |  |  | 0.779 | 0.250 |  |  |  |  |  |  |  |  |  |
|  |  | 0.914 |  |  |  |  |  |  |  | 0.9 |  |  |  |  |  |  |  |


| $\stackrel{\rightharpoonup}{6}$ |  | 感寺志思 | 䓘 |  |
| :---: | :---: | :---: | :---: | :---: |
|  | MNNNNN <br> 守品永肙 <br> 우N $\sim_{N}^{\sim}$ | か우N <br> N゙ずロ～～ <br> 구N NN |  |  |
|  |  |  |  |  |
|  | 요N유 Nさ～タ： N～～～～～ | 은ํํ N <br> 옹 <br> N～N |  |  |
|  |  | ฟ무우 <br> No№N <br>  |  | $\mathbf{0 4 : 4 5}$ PM    <br> 198 558 $95: 45$ 99 <br> 0.868 0.918 0.635 0.000 |
| $\sum_{\alpha}$ |  |  |  |  |

National Data \＆Surveying Services

## Intersection Turning Movement Count

Location：N Armenia Ave \＆W Hillsborough Ave／US 92／SR 600
Control：Signalized

| NS／EW Streets： | Data－Cars |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | N Armenia Ave |  |  |  | N Armenia Ave |  |  |  | W Hillsborough Ave／US 92／SR 600 |  |  |  | W Hillsborough Ave／US 92／SR 600 |  |  |  |  |
| AM | NORTHBOUND |  |  |  | SOUTHBOUND |  |  |  | EASTBOUND |  |  |  | WESTBOUND |  |  |  |  |
|  |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | $\begin{gathered} \mathbf{N} L \\ \hline \end{gathered}$ | NT | NR | NU | SL | 51 | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 7：00 AM | 20 | 36 | 13 | 0 | 29 | 62 | 13 | 0 | 27 | 351 | 37 | 1 | 11 | 401 | 11 | 1 | 1013 |
| 7：15 AM | 47 | 45 | 22 | 0 | 56 | 120 | 24 | 0 | 42 | 357 | 22 | 0 | 35 | 387 | 10 | 2 | 1169 |
| 7：30 AM | 39 | 62 | 31 | 0 | 69 | 138 | 26 | 0 | 31 | 359 | 47 | 5 | 44 | 443 | 10 | 3 | 1307 |
| 7：45 AM | 38 | 72 | 29 | 0 | 36 | 123 | 16 | 1 | 28 | 367 | 42 | 0 | 49 | 492 | 6 | 5 | 1304 |
| 8：00 AM8：15 AM8：30 AM8：45 AM | 40 | 71 | 15 | 0 | 36 | 136 | 14 | 0 | 35 | 355 | 52 | 2 | 44 | 411 | 16 | 0 | 1227 |
|  | 40 | 68 | 21 | 0 | 33 | 138 | 25 | 0 | 35 | 295 | 37 | 1 | 28 | 388 | 18 | 1 | 1128 |
|  | 30 | 43 | 23 | 0 | 36 | 114 | 21 | 1 | 31 | 333 | 33 | 4 | 35 | 471 | 15 | 2 | 1192 |
|  | 24 | 41 | 13 | 0 | 20 | 117 | 19 | 0 | 25 | 336 | 48 | 4 | 36 | 370 | 15 | 4 | 1072 |
| TOTAL VOLUMES ： <br> APPROACH \％＇s ： | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
|  | 278 | 438 | 167 | 0 | 315 | 948 | 158 | 2 | 254 | 2753 | 318 | 17 | 282 | 3363 | 101 | 18 | 9412 |
|  | 31．48\％ | 49．60\％ | 18．91\％ | 0．00\％ | 22．14\％ | 66．62\％ | 11．10\％ | 0．14\％ | 7．60\％ | 82．38\％ | 9．52\％ | 0．51\％ | 7．49\％ | 89．35\％ | 2．68\％ | 0．48\％ |  |
| PEAK HR： | 07：15 AM－08：15 AM |  |  |  | $\begin{aligned} & 197 \\ & 0.714 \end{aligned}$ | $\begin{aligned} & 517 \\ & 0.937 \end{aligned}$ | $\begin{gathered} 80 \\ 0.769 \end{gathered}$ | $\begin{gathered} 1 \\ 0.250 \end{gathered}$ | $\begin{aligned} & 136 \\ & 0.810 \end{aligned}$ | $\begin{gathered} 1438 \\ 0.980 \\ 0 \end{gathered}$ | $\begin{aligned} & 163 \\ & 0.784 \end{aligned}$ | $\begin{gathered} 7 \\ 0.350 \end{gathered}$ | $\begin{aligned} & 172 \\ & 0.878 \end{aligned}$ | $\begin{aligned} & 1733 \\ & 0.881 \end{aligned}$ | $\begin{gathered} 42 \\ 0.656 \end{gathered}$ | $\begin{gathered} 10 \\ 0.500 \end{gathered}$ | $\begin{aligned} & \text { TOTAL } \\ & 5007 \\ & 0.958 \\ & \hline \end{aligned}$ |
| PEAK HR VOL： | 164 | 250 | 97 | 0 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| PEAK HR FACTOR ： | 0.872 | 0.868 | 0.782 | 0.000 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| PEAKHRFACTOR： |  | 0.919 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


| $\stackrel{\square}{8}$ | 밍 욱 N N |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | M～～～～ <br>  <br> ～～～～～NN | 寸 ${ }^{(1) N}$ $\underset{\sim}{\underset{\sim}{\sim}} \underset{\sim}{\sim}$ <br> NMNN |  |  |
|  |  |  |  |  |
|  | 우N M m たツ゚ふ <br> Ñ | 은ㄴN <br> 응요 <br> N 네N NN |  |  |
|  |  <br> 〇ロ ロ～ G M M in | 누N 웅우 <br> 욱 $\overbrace{}^{\circ}$ <br> $\rightarrow-1$ <br> 今合俞 |  |  |
| $\sum_{\mathrm{L}}$ |  |  |  |  |

## Intersection Turning Movement Count

Location: N Armenia Ave \& W Hillsborough Ave/US 92/SR 600
Control: Signalized



## Intersection Turning Movement Count

Location: N Armenia Ave \& W Hillsborough Ave/US 92/SR 600
City: Tampa
Control: Signalized

| NS/EW Streets: | Data - Bikes |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $N$ Armenia Ave |  |  |  | $N$ Armenia Ave |  |  |  | W Hillsborough Ave/US 92/SR 600 |  |  |  | W Hillsborough Ave/US 92/SR 600 |  |  |  |  |
| AM | NORTHBOUND |  |  |  | SOUTHBOUND |  |  |  | EASTBOUND |  |  |  | WESTBOUND |  |  |  | TOTAL |
|  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $0$ | 0 | 0 |  |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU |  |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 3 |
| 7:45 AM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 2 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 |
| 8:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 3 |
| 8:45 AM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| TOTAL VOLUMES : APPROACH \%'S : |  | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
|  | $\begin{gathered} \mathrm{NL} \\ 0 \end{gathered}$ | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 5 | 0 | 0 |  | 6 | $0$ | $0$ | 17 |
|  | 0.00\% | 100.00\% | 0.00\% | 0.00\% | 0.00\% | 0.00\% | 100.00\% | 0.00\% | 28.57\% | 71.43\% | 0.00\% | 0.00\% | 0.00\% | 100.00\% | 0.00\% | 0.00\% |  |
| PEAK HR : | 07:15 AM - 08:15 AM |  |  |  | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | 00.0000 | $\begin{gathered} \quad \begin{array}{c} 1 \\ 0.250 \\ 0 \end{array} \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 1 \\ 0.250 \end{gathered}$ | $\begin{gathered} 2 \\ 0.500 \\ 0 . \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 2 \\ 0.500 \\ 0.500 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \\ 0 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 7 \\ 0.583 \\ \hline \end{gathered}$ |
| PEAK HR VOL: | 0 | 1 | 0 | 0 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| PEAK HR FACTOR : | 0.000 | 0.250 | 0.000 | 0.000 |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | 0.250 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


| $\frac{1}{5}$ | NM+60 | OmNN |  | $\frac{1}{\mathbf{1}} \approx \stackrel{\circ}{\mathrm{O}}$ |
| :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{cc} 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 3 & 0 \\ 0 & 0 \\ 0 & 0 \\ 3 & 0 \end{array}$ |  | 0000 <br> $00-10$ <br> NHNO <br> 0000 |  |  |
|  |  | 0000 <br> $-1007$ <br> NOOO |  |  |
|  |  | 0000 <br> ○~サー <br> 0000 |  |  |
|  |  | 0000 <br> 0000 <br> rooo |  | $04: 45$ PM    <br> 1 0 $05: 45 \mathrm{PM}$  <br> 0.250 0.000 0.000 0 <br>  0.250   |
| $\sum_{\Lambda}$ |  |  |  |  |

National Data \＆Surveying Services
Intersection Turning Movement Count
Project ID：23－120441－001
Location：Tampa
City：
Date：10／24／2023


| $\begin{gathered} 0 S \angle 0 \\ \star 乙 \\ 7 \forall \perp \perp \perp \end{gathered}$ | OSS＇0 |  | 0sz＇0 |  | OSS ${ }^{\circ}$ |  | 0SZ＇0 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\underset{L}{\varepsilon 8 c^{\circ} 0}$ | $\underset{\downarrow}{00 S^{\circ} 0}$ | $\begin{gathered} \text { OSZ:0 } \\ \text { I } \end{gathered}$ | 0 | $\begin{gathered} 8 \varepsilon t^{\circ} 0 \\ L \end{gathered}$ | $\underset{\downarrow}{\text { osz'0 }}$ | 0 | $\begin{gathered} \text { OSZ'0 } \\ \text { I } \\ \hline \end{gathered}$ |  |
|  |  |  |  |  |  |  | Wd St：S0－Wd St：to |  |  |
| 9S $7 \rightarrow \perp 0 \perp$ | $\begin{gathered} \% 00.08 \\ 0 z \\ \text { gS } \end{gathered}$ | $\begin{gathered} \% 00.02 \\ \mathrm{~s} \\ \text { gN } \\ \hline \end{gathered}$ | $\begin{gathered} \text { \%\&t'TL } \\ \mathrm{g} \\ \text { gS } \end{gathered}$ | $\begin{gathered} \text { \%LS'8Z } \\ Z \\ \text { gN } \end{gathered}$ | $\begin{gathered} \hline \% 68 \angle \angle \\ I I \\ \text { GM } \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { \%II'zt } \\ 8 \\ \text { gヨ } \\ \hline \end{gathered}$ | $\begin{gathered} \hline \% 00.0 t \\ 2 \\ \text { QM } \\ \hline \end{gathered}$ | $\begin{gathered} \% 00.09 \\ \varepsilon \\ 9 \exists \\ \hline \end{gathered}$ | ：s，\％HכVOYddy ：SヨWกาON 7VIOL |
| $\downarrow$ | 0 | 0 | 0 | 1 | 1 | 0 | 1 | 1 | Wd St：${ }_{\text {S }}$ |
| 5 | 1 | 1 | 1 | 0 | 1 | 0 | 0 | 1 | Wd 0E：S |
| 8 | 乙 | 1 | 0 | 0 | I | $\dagger$ | 0 | 0 | Wd St：${ }^{\text {S }}$ |
| 9 | $\varepsilon$ | 2 | 0 | 0 | I | 0 | 0 | 0 | Wd 00： 5 |
| 5 | 1 | 0 | 0 | 0 | t | 0 | 0 | 0 | Wd St：t |
| 9 | 0 | I | 2 | 0 | 1 | 1 | 0 |  | Wd 0¢：${ }^{\text {b }}$ |
| 85 | $\varepsilon \downarrow$ | 0 | 0 | 0 | て | $\varepsilon$ |  | 0 | Wd SI：${ }^{\text {b }}$ |
| b |  | 0 | 2 | 1 | 0 | 0 | 1 | 0 | Wd 00：b |
| 7 7101 | $\begin{aligned} & 8 \mathrm{~S} \\ & \hline 93 \end{aligned}$ | ${ }^{9 \times}{ }^{9 N}$ | $9$ |  | $\begin{aligned} & \hline 9 M \\ & \hline 97 \end{aligned}$ | $\begin{array}{r} 9 \exists \\ \mathrm{nOS} \\ \hline \end{array}$ | $\begin{aligned} & \hline 9 M \\ & \hline 971 \end{aligned}$ | $\begin{array}{r} 9 \exists \\ -\mathrm{yON} \\ \hline \end{array}$ | Wd |





Prepared by National Data \& Surveying Services
N Rome Ave \& W Hillsborough Ave/US 92/SR 600
Peak Hour Turning Movement Count


## Intersection Turning Movement Count

Location: N Rome Ave \& W Hillsborough Ave/US 92/SR 600
Control: Signalized

| Data - Total |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NS/EW Streets: | N Rome Ave |  |  |  | N Rome Ave |  |  |  | W Hillsborough Ave/US 92/SR 600 |  |  |  | W Hillsborough Ave/US 92/SR 600 |  |  |  |  |
| AM | NORTHBOUND |  |  |  | SOUTHBOUND |  |  |  | EASTBOUND |  |  |  | WESTBOUND |  |  |  |  |
|  | 0 | $0$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | $0$ | $0$ | $0$ | 0 | 0 | 0 |  |
|  | NL | NT | NR | NU | SL | ST | SR | SU | $\mathrm{EL}$ | $E T$ | ER | EU | WL | WT | WR | WU | TOTAL |
| 7:00 AM | 19 | 20 | 18 | 0 | 22 | 43 | 21 | 0 | 4 | 315 | 21 | 12 | 6 | 415 | 7 | 0 | 923 |
| 7:15 AM | 13 | 37 | 11 | 0 | 26 | 55 | 29 | 0 | 11 | 396 | 25 | 25 | 13 | 503 | 13 | 0 | 1157 |
| 7:30 AM | 30 | 46 | 17 | 0 | 20 | 49 | 19 | 0 | 14 | 411 | 64 | 18 | 25 | 511 | 14 | 1 | 1239 |
| 7:45 AM | 33 | 37 | 17 | 0 | 40 | 77 | 20 | 0 | 11 | 351 | 57 | 11 | 20 | 423 | 11 | 0 | 1108 |
| 8:00 AM | 34 | 29 | 17 | 0 | 40 | 43 | 25 | 0 | 16 | 396 | 29 | 7 | 19 | 437 | 17 | 0 | 1109 |
| 8:15 AM | 15 | 17 | 12 | 0 | 34 | 46 | 23 | 0 | 10 | 372 | 11 | 7 | 11 | 490 | 11 | 1 | 1060 |
| 8:30 AM | 19 | 23 | 17 | 0 | 32 | 40 | 25 | 0 | 14 | 353 | 15 | 5 | 8 | 404 | 15 | 0 | 970 |
| 8:45 AM | 21 | 20 | 11 | 0 | 29 | 49 | 21 | 0 | 16 | 337 | 11 | 7 | 9 | 377 | 13 | 0 | 921 |
|  |  | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
|  | 184 | 229 | 120 | 0 | 243 | 402 | 183 | 0 | 96 | 2931 | 233 | 92 | 111 | 3560 | 101 | 2 | 8487 |
| APPROACH \%'s : | 34.52\% | 42.96\% | 22.51\% | 0.00\% | 29.35\% | 48.55\% | 22.10\% | 0.00\% | 2.86\% | 87.44\% | 6.95\% | 2.74\% | 2.94\% | 94.33\% | 2.68\% | 0.05\% |  |
| PEAK HR: | 07:15 AM - 08:15 AM |  |  |  | $\begin{aligned} & 126 \\ & 0.788 \end{aligned}$ | 224 | $\begin{gathered} 93 \\ 0.802 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 52 \\ 0.813 \end{gathered}$ | $\begin{aligned} & 1554 \\ & 0.945 \end{aligned}$ | $\begin{aligned} & 175 \\ & 0.684 \end{aligned}$ | $\begin{gathered} 61 \\ 0.610 \end{gathered}$ | $\begin{gathered} 77 \\ 0.770 \end{gathered}$ | $\begin{aligned} & 1874 \\ & 0.917 \end{aligned}$ | $\begin{gathered} 55 \\ 0.809 \end{gathered}$ | $\begin{gathered} 1 \\ 0.250 \end{gathered}$ | $\begin{aligned} & \text { TOTAL } \\ & 4613 \\ & 0.931 \\ & \hline \end{aligned}$ |
| PEAK HR VOL: | 110 | 149 | 62 | 0 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| PEAK HR FACTOR : | 0.809 | 0.810 | 0.912 | 0.000 |  | 0.727 |  |  |  |  |  |  |  |  |  |  |  |
|  |  | 0.863 |  |  |  | 0.808 |  |  |  |  |  |  |  |  |  |  |  |


National Data \& Surveying Services
Intersection Turning Movement Count
Location: N Rome Ave \& W Hillsborough Ave/US 92/SR 600
City: Tampa
Control: Signalized

| NS/EW Streets: | Data - Cars |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | N Rome Ave |  |  |  | N Rome Ave |  |  |  | W Hillsborough Ave/US 92/SR 600 |  |  |  | W Hillsborough Ave/US 92/SR 600 |  |  |  |  |
| AM | NORTHBOUND |  |  |  | SOUTHBOUND |  |  |  | EASTBOUND |  |  |  | WESTBOUND |  |  |  | TOTAL |
|  | $0$ | NT | 0 | 0 | 0SL | 0ST | $\begin{gathered} 0 \\ \text { SR } \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ S U \end{gathered}$ | EL |  | 0 | 0 | $\begin{gathered} 0 \\ \mathrm{WL} \end{gathered}$ | $\begin{gathered} 0 \\ \text { WT } \end{gathered}$ | $\stackrel{0}{\text { WR }}$ | $\begin{gathered} 0 \\ \text { wu } \end{gathered}$ |  |
|  |  |  | NR | NU |  |  |  |  |  |  | ER | EU |  |  | WR |  |  |
| 7:00 AM | 17 | 20 | 16 | 0 | 21 | 41 | 21 | 0 | 4 | ET | 20 | 11 | 513 | 403488 | 6 | 0 | 882 |
| 7:30 AM | 12 | 36 | 10 | 0 | 25 | 54 | 29 | 0 | 11 | 371 | 25 | 25 |  |  | 14 | 0 | 1111 |
|  | 30 | 45 | 15 | 0 | 20 | 48 | 18 | 0 | 13 | 393 | 64 | 18 | 25 | 487 |  | 1 | 11911069 |
| 7:45 AM | 32 | 36 | 17 | 0 | 39 | 75 | 19 | 0 | 11 | 336 | 57 | 11 | 20 | 406 | 10 |  |  |
| 8:00 AM | 33 | 29 | 17 | 0 | 40 | 42 | 24 | 0 | 16 | 371 | 29 | 7 | 19 | 414 | 17 | 0 | $\begin{aligned} & 1058 \\ & 990 \\ & 911 \\ & 871 \end{aligned}$ |
| 8:15 AM | 14 | 16 | 11 | 0 | 33 | 45 | 23 | 0 | 10 | 348 | 11 | 6 | 8 | 456 | 14 | 1 |  |
| 8:30 AM8:45 AM | 15 | 23 | 14 | 0 | 31 | 36 | 25 | 0 | 14 | 328 | 15 | 4 | 8 | 384 |  | 0 |  |
|  | 19 | 18 | 11 | 0 | 27 | 47 | 21 | 0 | 14 | 317 | 10 | 7 | 9 | 359 | 12 | 871 |  |
| TOTAL VOLUMES : APPROACH \%'s : | NL NT NR NU |  |  |  | $\begin{gathered} \text { SL } \\ 236 \\ 29.35 \% \\ \hline \end{gathered}$ | $\begin{gathered} \text { ST } \\ 388 \\ 48.26 \% \\ \hline \end{gathered}$ | $\begin{gathered} \text { SR } \\ 180 \\ 22.39 \% \\ \hline \end{gathered}$ | $\begin{array}{l\|} \hline \text { SU } \\ 0 \\ 0.00 \% \\ \hline \end{array}$ | $\begin{aligned} & \hline \text { EL } \\ & 93 \\ & 2.93 \% \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { ET } \\ & 2761 \\ & 86.99 \% \end{aligned}$ | $\begin{aligned} & \hline \text { ER } \\ & 231 \\ & 7.28 \% \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \text { EU } \\ & 89 \\ & 2.80 \% \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \text { WL } \\ & 107 \\ & 2.97 \% \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { WT } \\ & 3397 \\ & 94.39 \% \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \text { WR } \\ & 93 \\ & 2.58 \% \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { WU } \\ & 2 \\ & 0.06 \% \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \text { TOTAL } \\ & 8083 \end{aligned}$ |
|  | 172 | 223 | 111 | 0 |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 33.99\% | 44.07\% | 21.94\% | 0.00\% |  |  |  |  |  |  |  |  |  |  |  |  |  |
| PEAK HR: | 07:15 AM - 08:15 AM |  |  |  | $\begin{aligned} & 124 \\ & 0.775 \end{aligned}$ | $\begin{aligned} & 219 \\ & 0.730 \end{aligned}$ | $\begin{gathered} 90 \\ 0.776 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 51 \\ 0.797 \end{gathered}$ | $\begin{aligned} & 1471 \\ & 0.936 \end{aligned}$ | $\begin{aligned} & 175 \\ & 0.684 \end{aligned}$ | $\begin{gathered} 61 \\ 0.610 \end{gathered}$ | $\begin{gathered} 77 \\ 0.770 \end{gathered}$ | $\begin{aligned} & 1795 \\ & 0.920 \end{aligned}$ | $\begin{gathered} 53 \\ 0.779 \end{gathered}$ | $\begin{gathered} 1 \\ 0.250 \end{gathered}$ | $\begin{aligned} & \text { TOTAL } \\ & 4429 \\ & 0.930 \end{aligned}$ |
| PEAK HR VOL : | 107 | 146 | 59 | 0 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| PEAK HR FACTOR : | 0.811 | 0.811 | 0.868 | 0.000 |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | ${ }_{0.867} 0.8$ |  |  |  |  | 0.814 |  |  |  |  |  |  |  |  |  |  |  |



## Intersection Turning Movement Count

Location: N Rome Ave \& W Hillsborough Ave/US 92/SR 600
Control: Signalized

| NS/EW Streets: | Data - HT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | N Rome Ave |  |  |  | $N$ Rome Ave |  |  |  | W Hillsborough Ave/US 92/SR 600 |  |  |  | W Hillsborough Ave/US 92/SR 600 |  |  |  |  |
| AM | NORTHBOUND |  |  |  | SOUTHBOUND |  |  |  | EASTBOUND |  |  |  | WESTBOUND |  |  |  |  |
|  |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | $\mathrm{NL}$ | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 7:00 AM | 2 | 0 | 2 | 0 | 1 | 2 | 0 | 0 | 0 | 18 | 1 | 1 | 1 | 12 | 1 | 0 | 41 |
| 7:15 AM | 1 | 1 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 25 | 0 | 0 | 0 | 15 | 1 | 0 | 46 |
| 7:30 AM | 0 | 1 | 2 | 0 | 0 | 1 | 1 | 0 | 1 | 18 | 0 | 0 | 0 | 24 | 0 | 0 | 48 |
| 7:45 AM | 1 | 1 | 0 | 0 | 1 | 2 | 1 | 0 | 0 | 15 | 0 | 0 | 0 | 17 | 1 | 0 | 39 |
| 8:00 AM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 25 | 0 | 0 | 0 | 23 | 0 | 0 | 51 |
| 8:15 AM | 1 | 1 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 24 | 0 | 1 | 3 | 34 | 3 | 0 | 70 |
| 8:30 AM | 4 | 0 | 3 | 0 | 1 | 4 | 0 | 0 | 0 | 25 | 0 | 1 | 0 | 20 | 1 | 0 | 59 |
| 8:45 AM | 2 | 2 | 0 | 0 | 2 | 2 | 0 | 0 | 2 | 20 | 1 | 0 | 0 | 18 | 1 | 0 | 50 |
|  |  |  |  |  |  | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
|  | $\begin{aligned} & \text { NL } \\ & 12 \end{aligned}$ | $\begin{gathered} \mathrm{N} 1 \\ 6 \end{gathered}$ | $\begin{gathered} \text { NR } \\ 9 \end{gathered}$ | 0 | 7 | 14 | 3 | 0 | 3 | 170 | 2 | 3 | 4 | 163 | 8 | 0 | 404 |
| TOTAL VOLUMES : | 44.44\% | 22.22\% | 33.33\% | 0.00\% | 29.17\% | 58.33\% | 12.50\% | 0.00\% | 1.69\% | 95.51\% | 1.12\% | 1.69\% | 2.29\% | 93.14\% | 4.57\% | 0.00\% |  |
| APPROACH \%'S : | 07:15 AM - 08:15 AM |  |  |  | $\begin{gathered} 2 \\ 0.500 \end{gathered}$ | $\begin{gathered} 5 \\ 0.625 \\ 0 . \end{gathered}$ | $\begin{gathered} 3 \\ 0.750 \\ 5 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 1 \\ 0.250 \end{gathered}$ | $\begin{gathered} 83 \\ 0.830 \\ 0 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 79 \\ 0.823 \end{gathered}$ | $\begin{gathered} 2 \\ 4^{2} .500 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ |  <br> TOTAL <br> 184 <br> 0.902 |
| PEAK HR VOL : | 3 | 3 | 3 | 0 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| PEAK HR FACTOR : | 0.750 | 0.750 | 0.375 | 0.000 |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | 0.750 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


| $\stackrel{\rightharpoonup}{6}$ | m | 앙NN | $\frac{1}{6}$ |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | $N-1+-1$ $\underset{\sim}{\infty} \underset{\sim}{\infty} \underset{\sim}{\top}$ <br> $700-$ |  |  |
|  |  | $1000$ $\underset{\sim}{\wedge} \infty$ <br> 0007 |  |  |
|  |  | $00 \text {-10 }$ <br> $+-4 \quad+-4 \quad+0+1$ <br> $0-1+0$ |  |  |
|  |  | 0000 <br> 0 -1 -1 <br> 0000 |  |  |
| $\frac{\sum}{\Omega}$ |  |  |  |  |

National Data \& Surveying Services

## Intersection Turning Movement Count

Location: N Rome Ave \& W Hillsborough Ave/US 92/SR 600
Control: Signalized

| Data - Bike |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NS/EW Streets: | N Rome Ave |  |  |  | N Rome Ave |  |  |  | W Hillsborough Ave/US 92/SR 600 |  |  |  | W Hillsborough Ave/US 92/SR 600 |  |  |  |  |
| AM | NORTHBOUND |  |  |  | SOUTHBOUND |  |  |  | EASTBOUND |  |  |  | WESTBOUND |  |  |  | TOTAL |
|  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU |  |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 3 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 |
| 8:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  |  | NT | NR | NU | SL. | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | $0$ | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 4 | $0$ | $0$ | 9 |
| APPROACH \%'S : | 0.00\% | 100.00\% | 0.00\% | 0.00\% | 0.00\% | 100.00\% | 0.00\% | 0.00\% | 0.00\% | 100.00\% | 0.00\% | 0.00\% | 0.00\% | 100.00\% | 0.00\% | 0.00\% |  |
| PEAK HR: |  | 07:15 AM - | 8:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  | TOTAL |
| PEAK HR VOL: | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 1 |  | 0 | 6 |
| PEAK HR FACTOR : | 0.000 | 0.250 | 0.000 | 0.000 | 0.000 | 0.250 | 0.000 | 0.000 | 0.000 | 0.375 | 0.000 | 0.000 | 0.000 | 0.250 | 0.000 | 0.000 | 0.500 |
| PEAK HR PACTOR. |  | 0.2 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


| $\stackrel{1}{5}$ | mrotm | $\rightarrow \mathrm{mm}$ | $\left\|\begin{array}{ll} \frac{1}{\widehat{人}} & 0 \\ \stackrel{\rightharpoonup}{6} & -1 \end{array}\right\|$ |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | 0000 <br> $\rightarrow$ - N <br> 0000 |  |  |
|  |  | 0000 <br> 0 -roo <br> OOनO |  |  |
|  |  | $0-100$ <br> 0000 <br> 0000 |  |  |
|  |  | 0000 <br> 0000 <br> 0000 | $\begin{array}{\|cc\|} \hline 2 & 0 \\ 2 & 0 \\ \hline \end{array}$ |  |
| $\sum_{2}$ |  |  |  |  |

National Data \＆Surveying Services
Intersection Turning Movement Count
Location：N Rome Ave \＆W Hillsborough Ave／US 92／SR $600 \quad$ Project ID：23－120441－002 City：Tampa
Data－Pedestrians（Crosswalks）

| NS／EW Streets： | Data－Pedestrians（Crosswalks） |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | N Rome Ave |  | N Rome Ave |  | W Hillsborough Ave／US 92／SR 600 |  | W Hillsborough Ave／US 92／SR 600 |  |  |
| AM | NORTH LEG |  | SOUTH LEG |  | EAST LEG |  | WEST LEG |  | TOTAL |
|  | EB | WB | EB | WB | NB | SB | NB | SB |  |
| 7：00 AM | 0 | 1 |  | 0 | 0 | 0 | 1 | 0 | 4 |
| 7：15 AM | 0 | 1 | 0 | 2 | 0 | 0 | 1 | 0 | 4 |
| 7：30 AM | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 |
| 7：45 AM | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 3 |
| 8：00 AM | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 3 |
| 8：15 AM | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 2 | 4 |
| 8：30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8：45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL VOLUMES ： APPROACH \％＇s ： | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
|  | 3 | 4 | 4 | 3 | 1 | 0 | 2 | 4 | 21 |
|  | 42．86\％ | 57．14\％ | 57．14\％ | 42．86\％ | 100．00\％ | 0．00\％ | 33．33\％ | 66．67\％ |  |
| PEAK HR ： | 07：15 AM－08：15 AM |  | $\begin{gathered} 2 \\ 0.250 \end{gathered}$ | ${ }_{0.500} \begin{gathered} 2 \\ 0.250 \end{gathered}$ | $\begin{gathered} 1 \\ 0.250 \end{gathered}$ | 0 | $\begin{gathered} 1 \\ 0.250 \end{gathered}$ | ${ }_{0.750} \begin{gathered} 2 \\ 0.500 \\ \hline \end{gathered}$ | TOTAL |
| PEAK HR VOL： | 3 | 2 |  |  |  |  |  |  | 13 |
| PEAK HR FACTOR ： | 0.375 | 0.500 |  |  |  |  |  |  | 0.813 |
|  | 0.625 |  |  |  |  |  |  |  | 0.813 |


| $\begin{gathered} 669^{\circ} 0 \\ \mathrm{Sz} \\ 7 \forall \perp 10 \perp \end{gathered}$ | 00G＇0 |  | દعદ＊0 |  | 00S＇0 |  | OSE＇0 |  | ：yOLOVA 8H XVヨd <br> ：701 ४H XVヨd |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\underset{\downarrow}{00 s^{\circ} 0}$ | $\underset{\downarrow}{\varepsilon \varepsilon \varepsilon} \cdot 0$ | 0 | $\underset{\downarrow}{\varepsilon \varepsilon \varepsilon^{\prime} 0}$ | $\underset{\succ}{\varepsilon \varepsilon \varepsilon^{\prime} 0}$ | $\begin{gathered} \text { OSZ"0 } \\ Z \end{gathered}$ | $\underset{\varepsilon}{0 S}{ }_{\varepsilon}^{\circ}$ | $\begin{gathered} \text { OsZ'0 } \\ \downarrow \\ \hline \end{gathered}$ |  |
|  |  |  |  |  |  |  |  |  |  |
| $\stackrel{\angle b}{7 \forall \perp 1}$ | $\begin{gathered} \text { \% } \% 8^{\prime} 9 \varepsilon \\ L \\ \text { gS } \end{gathered}$ | $\begin{gathered} \hline \text { \%91' } \quad \text { 29 } \\ \text { ZI } \\ \text { QN } \\ \hline \end{gathered}$ | $\begin{gathered} \text { \%00'0 } \\ 0 \\ \text { gS } \\ \hline \end{gathered}$ | $\begin{gathered} \hline \% 0^{\prime} 00 \tau \\ \quad \\ \text { gN } \\ \hline \end{gathered}$ | $\begin{gathered} \text { \% } \varepsilon \varepsilon \cdot \varepsilon \varsigma \\ 8 \\ 8 M \\ \hline \end{gathered}$ | $\begin{gathered} \text { \% } \angle 9.9 t \\ L \\ \text { Qヨ } \\ \hline \end{gathered}$ | $\begin{gathered} \text { \%99'SS } \\ 5 \\ \text { gM } \\ \hline \end{gathered}$ | $\begin{gathered} \text { \% }+t^{\prime}+t \\ \quad \\ \text { g } \\ \hline \end{gathered}$ |  |
| S | 0 | $\varepsilon$ | 0 | 0 | 乙 | 0 | 0 | 0 | Wd St：${ }^{\text {S }}$ |
| G | 0 | 0 | 0 | $\varepsilon$ | 1 | 0 | 1 | 0 | Wd 0¢： |
| 6 | I | $\varepsilon$ | 0 | 0 | 0 | 0 | I | $\dagger$ | Wd St：${ }^{\text {S }}$ |
| ¢ | て | 0 | 0 | 0 | $\varepsilon$ | 0 | 0 | 0 | Wd 00：S |
| 9 | 1 | I | 0 | 1 | 0 | Z | 1 | 0 | Wd St：t |
| 9 | て | 1 | 0 | 0 | ， | て | 0 | 0 | Wd $0 \varepsilon: 7$ |
| $\downarrow$ | 0 | 2 | 0 | 0 | 0 | I | I | 0 | Wd ST：$\downarrow$ |
| $\angle$ | 1 | 2 | 0 | 0 | 1 | 2 | 1 | 0 | Wd 00： t |
| 78101 | $\begin{aligned} & 9 \mathrm{~g} \\ & \hline 9 \end{aligned}$ | ${ }^{9 N}$ |  | ${ }^{1 S V I}{ }^{9 N}$ | $\begin{gathered} 9 M \\ 93 \\ \hline \end{gathered}$ | $\begin{gathered} { }^{93} \\ \mathrm{LnOs} \\ \hline \end{gathered}$ | $\begin{aligned} & 9 M \\ & \hline \end{aligned}$ | ${ }^{\text {LYON }}$ | Wd |





E/W Street: W Hillsborough Ave/US 92/SR 600


National Data \& Surveying Services
Site Code: 23-120441-003


## Aunns



## Hillsborough 07:00-09:00 16:00-18:00 <br> pez!ןeus!s <br> Count Times: Control:

SIGNAL TIMING

| PHASES | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ |
| :--- | :---: | :---: | :---: |
| NT/ST | $00: 19$ | $00: 20$ | $00: 19$ |
| WL/WT | $00: 21$ | $00: 13$ | $00: 17$ |
| ET/WT | $02: 26$ | $02: 34$ | $02: 43$ |
| EL/ET | $00: 13$ | $00: 14$ | - |

Prepared by National Data \& Surveying Services
N Lee Pl \& W Hillsborough Ave/US 92/SR 600
Peak Hour Turning Movement Count

ID: 23-120441-003
City: Tampa


Cars (NOON)


Cars (PM)



SOUTHBOUND

| AM | 0 | 5 | 44 | 0 | 7 | AM |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NOON | 0 | 0 | 0 | 0 | 0 | NOON |
| PM | 3 | 0 | 12 | 0 | 20 | PM |

Day: Tuesday
Date: 10/24/2023


HT (NOON)


HT (PM)



National Data \＆Surveying Services

## Intersection Turning Movement Count

Location：N Lee PI \＆W Hillsborough Ave／US 92／SR 600 Control：Signalized

| NS／EW Streets： | N Lee Pl |  |  |  | N Lee Pl |  |  |  | W Hillsborough Ave／US 92／SR 600 |  |  |  | W Hillsborough Ave／US 92／SR 600 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM | NORTHBOUND |  |  |  | SOUTHBOUND |  |  |  | EASTBOUND |  |  |  | WESTBOUND |  |  |  | TOTAL |
|  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU |  |
| 7：00 AM | 7 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 329 | 1 | 0 | 5 | 459 | 0 | 1 | 804 |
| 7：15 AM | 5 | 0 | 2 | 0 | 3 | 0 | 0 | 0 | 1 | 385 | 0 | 1 | 9 | 560 | 2 | 3 | 971 |
| 7：30 AM | 8 | 0 | 0 | 0 | 10 | 2 | 0 | 0 | 0 | 484 | 1 | 1 | 17 | 521 | 1 | 3 | 1048 |
| 7：45 AM | 7 | 0 | 1 | 0 | 21 | 1 | 0 | 0 | 0 | 394 | 4 | 1 | 22 | 487 | 1 | 5 | 944 |
| 8：00 AM | 0 | 2 | 2 | 0 | 10 | 2 | 0 | 0 | 0 | 408 | 0 | 1 | 9 | 530 | 0 | 0 | 964 |
| 8：15 AM | 2 | 0 | 2 | 0 | 9 | 0 | 0 | 0 | 0 | 424 | 3 | 2 | 8 | 474 | 2 | 3 | 929 |
| 8：30 AM | 6 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 396 | 1 | 0 | 6 | 434 | 1 | 2 | 850 |
| 8：45 AM | 5 | 0 | 0 | 0 | 3 | 0 | 2 | 0 | 0 | 327 | 3 | 2 | 5 | 458 | 2 | 5 | 812 |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES： | 40 | 2 | 7 | 0 | 62 | 5 | 2 | 0 | 1 | 3147 | 13 | 8 | 81 | 3923 | 9 | 22 | 7322 |
| APPROACH \％＇s ： | 81．63\％ | 4．08\％ | 14．29\％ | 0．00\％ | 89．86\％ | 7．25\％ | 2．90\％ | 0．00\％ | 0．03\％ | 99．31\％ | 0．41\％ | 0．25\％ | 2．01\％ | 97．22\％ | 0．22\％ | 0．55\％ |  |
| PEAK HR ： | 07：15 AM－08：15 AM |  |  |  | $\begin{gathered} 44 \\ 0.524 \end{gathered}$ | $\begin{gathered} 5 \\ 0.625 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 1 \\ 0.250 \end{gathered}$ | $\begin{aligned} & 1671 \\ & 0.863 \end{aligned}$ | $\begin{gathered} 5 \\ 5^{5.313} \\ \hline \end{gathered}$ | $\begin{gathered} 4 \\ 1.000 \end{gathered}$ | $\begin{gathered} 57 \\ 0.648 \end{gathered}$ | $\begin{aligned} & 2098 \\ & 0.937 \end{aligned}$ | $\begin{gathered} 4 \\ 0.500 \end{gathered}$ | $\begin{gathered} 11 \\ 0.550 \end{gathered}$ | $\begin{aligned} & \text { TOTAL } \\ & 3927 \\ & 0.937 \end{aligned}$ |
| PEAK HR VOL ： | 20 | 2 | 5 | 0 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| PEAK HR FACTOR ： | 0.625 | 0.250 | 0.625 | 0.000 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| PEAK HR FACTOR |  | 0.844 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


|  |  | 发员 | 迫 |
| :---: | :---: | :---: | :---: |
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|  |  |  |  |
|  |  |  |  |
|  | 00000000 <br> VNMOVm $\infty$ N <br> 0000 HOMm <br>  |  |  |
| $\sum_{n}$ | $\sum_{n} \sum_{n} \sum_{n} \sum_{n} \sum_{i} \sum_{n} \sum_{i} \sum_{n}$ <br>  <br>  |  |  |

Location：N Lee PI \＆W Hillsborough Ave／US 92／SR 600
Control：Signalized


| $\stackrel{1}{6}$ | N M M N m ¢ | 강NN |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | M N N N <br> $-100-10$ | 0000 <br> 윽ํํ <br> 000 H |  |  |
|  | 0000 <br> －m <br> 0000 | 0000 <br>  <br> $-1000$ |  |  |
|  |  | 0000 <br> 0000 <br> 0000 |  | $0 \stackrel{8}{0}$ $08$ - <br> － 8 |
|  |  | 0000 <br> 0000 <br> 7000 | $\begin{array}{\|cc\|} \hline & 0 \\ 2 & 0 \\ \hline 2 & 0 \\ \hline \end{array}$ |  |
| $\sum_{\Lambda}$ |  |  |  |  |

National Data \＆Surveying Services
Intersection Turning Movement Count
Location：N Lee PI \＆W Hillsborough Ave／US 92／SR 600
City：Tampa
Control：Signalized

|  | Data－Bikes |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NS／EW Streets： | N Lee Pl |  |  |  | N Lee Pl |  |  |  | W Hillsborough Ave／US 92／SR 600 |  |  |  | W Hillsborough Ave／US 92／SR 600 |  |  |  |  |
| AM | NORTHBOUND |  |  |  | SOUTHBOUND |  |  |  | EASTBOUND |  |  |  | WESTBOUND |  |  |  |  |
|  | 0 | 0 | 0 | NU | $\begin{aligned} & 0 \\ & \mathrm{SL} \\ & \hline \end{aligned}$ | 0ST | 0 | 0 | O | $\begin{aligned} & 0 \\ & \text { ET } \end{aligned}$ | 0 | 0 | $\begin{gathered} 0 \\ \mathrm{WL} \end{gathered}$ | $\begin{gathered} 0 \\ \text { WT } \end{gathered}$ | 0 | $0$ |  |
|  | NL | NT | NR |  |  |  | SR | SU |  |  | ER | EU |  |  | WR |  |  |
| 7：00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 |
| 7：15 AM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 3 |
| 7：30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7：45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8：00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8：15 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 4 |
| 8：30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 8：45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  |  |  |  | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES： APPROACH \％＇s： | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 3 | 0 |  | 9 |
|  | 50．00\％ | 0．00\％ | 50．00\％ | 0．00\％ | 0．00\％ | 100．00\％ | 0．00\％ | 0．00\％ | 0．00\％ | 66．67\％ | 33．33\％ | 0．00\％ | 0．00\％ | 100．00\％ | 0．00\％ | 0．00\％ |  |
| PEAK HR： | 07：15 AM－08：15 AM |  |  |  | 0 | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ |  | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | 10.250 | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} \text { TOTAL } \\ 3 \\ 0.250 \end{gathered}$ |
| PEAK HR VOL： | 0 | 0 | 1 | 0 |  |  |  |  |  | 1 |  |  |  |  |  |  |  |
| PEAK HR FACTOR ： | 0.000 | 0.000 | 0.250 | 0.000 | $0.000$ |  |  |  |  | 0.250 |  |  |  |  |  |  |  |
|  | 0.250 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


| $\stackrel{\rightharpoonup}{6}$ | －momm | $m-m-1$ | 咎べ | 这へ |
| :---: | :---: | :---: | :---: | :---: |
|  |  | 0000 <br> －10NO <br> HOOO |  | ー～～썽 <br> $\rightarrow$－웅 |
| $\qquad$ |  | 0000 <br> $0 \rightarrow-$ <br> 0000 |  | $\bigcirc \stackrel{8}{0}$ <br> －$\stackrel{0}{0}$ -品 <br> $-\frac{8}{0}$ |
|  | 0000 <br> 0000 <br> 0000 | 0000 <br> 0000 <br> 0000 | $\begin{aligned} & \text { no } \\ & \text { no } \\ & \text { no } \\ & \text { no } \end{aligned}$ | －$\stackrel{8}{\circ}$ <br> $0 \stackrel{8}{0}$ <br> － <br> － 8 |
|  | 0000 <br> 0000 <br> 0000 | 0000 <br> 0000 | $\begin{aligned} & \frac{120}{20} \\ & \frac{x}{2} 0 \\ & \frac{1}{2} 0 \\ & \equiv 0 \end{aligned}$ |  |
| $\sum_{\alpha}$ |  |  |  |  |

National Data \＆Surveying Services Intersection Turning Movement Count
Location：N Lee PI \＆W Hillsborough Ave／US 92／SR 600 Project ID：23－120441－003 City：Tampa
Data－Pedestrians（Crosswalks）

| NS／EW Streets： | Data－Pedestrians（Crosswalks） |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | N Lee Pl |  | N Lee PI |  | W Hillsborough Ave／US 92／SR 600 |  | W Hillsborough Ave／US$92 /$ SR 600 |  |  |
| AM | NORTH LEG |  | SOUTH LEG |  | EAST LEG |  | WEST LEG |  |  |
|  | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| 7：00 AM | 0 | 1 |  | 0 | 2 | 0 | 0 | 0 | 4 |
| 7：15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7：30 AM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| 7：45 AM | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 3 |
| 8：00 AM | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 8：15 AM | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 8：30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8：45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL VOLUMES ： APPROACH \％＇s ： | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
|  | 2 | 1 | 2 | 1 | 2 | 0 | 2 | 0 | 10 |
|  | 66．67\％ | 33．33\％ | 66．67\％ | 33．33\％ | 100．00\％ | 0．00\％ | 100．00\％ | 0．00\％ |  |
| PEAK HR ： | 07：15 AM－08：15 AM |  | $\begin{gathered} 1 \\ 0.250 \end{gathered}$ | $0.500{ }^{\begin{array}{c} 1 \\ 0.250 \\ 0 \end{array}}$ | 0 | 0 | $\begin{gathered} 2 \\ 0.250 \end{gathered}$ | 0 | TOTAL |
| PEAK HR VOL： | 1 | 0 |  |  |  |  |  |  | 5 |
| PEAK HR FACTOR ： | 0.250 |  |  |  |  |  |  |  |  |
|  | 0.250 |  |  |  |  |  |  |  | 0.417 |


| $\begin{gathered} 005^{\circ} 0 \\ \stackrel{t}{7} \underset{\sim}{\mathrm{O}} \mathrm{O} \end{gathered}$ | 0 | 0 | 05Z＇0 |  | 00S ${ }^{\circ}$ |  | OSZ＇0 |  | ：YOLOVG YH X甘ヨd <br> ：701 YH XVヨd |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\underset{\text { OSZ }}{\text { OS }}$ | $\underset{\mathrm{L}}{\mathrm{OSZ}}$ | $\begin{gathered} \text { OSZ'0 } \\ \text { I } \end{gathered}$ | $\begin{gathered} \text { osz'0 } \\ \text { I } \\ \hline \end{gathered}$ | 0 |  |
|  |  |  |  |  |  |  | Wd 0¢：S0－Wd 0ع： 0 |  | ：8H XVヨd |
|  | \％00＇00T | \％00＇0 | \％00＇0 | \％00＇00T | \％عદ＇$\varepsilon \varepsilon$ | \％L9＇99 | \％00＇00I | \％00＇0 | ： S ，\％HOVOZddV <br> ：S3WกาON TVIOL |
| 6 | I | 0 | 0 | I | 乙 | b | I | 0 |  |
| 76101 | gS | gN | 9S | gN | 9 M | 83 | 9M | $8 \exists$ |  |
| I | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | Wd St：${ }^{\text {S }}$ |
| 1 | 1 | 0 | ， | 0 | 0 | 0 | 0 | 0 | Wd 0¢：${ }^{\text {c }}$ |
| I | 0 | 0 | 0 | 0 | I | 0 | 0 | 0 | Wd St： |
| 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | Wd 00：S |
| 2 | 0 | 0 | 0 | โ | 0 | I | 0 | 0 | Wd St： t |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | Wd 0¢：${ }^{\text {W }}$ |
| I | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | Wd SI： b |
| 2 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | Wd 00： t |
| $7 \forall 101$ | ${ }^{93}{ }^{9715 \exists M}{ }^{9 N}$ |  | 95 | ${ }^{\text {gN }}$ | $\mathrm{gM}_{9 \exists 7 \mathrm{H} \perp \mathrm{nOS}} \mathrm{~g}^{9 \exists}$ |  | $\begin{gathered} 9 M \\ 9 \exists 7 \mathrm{H} \perp 80 \mathrm{~N} \\ \hline \end{gathered}$ |  | Wd |
|  |  |  | 937 15Vヨ |  |  |  |  |  |  |  |




FDOT PEAK SEASON ADJUSTMENT FACTORS


SIGNAL TIMING SHEETS

## 609 Timing Date: <br> $\begin{array}{ll}\text { Major Street } & \text { HILLSBOROUGH } \\ \text { Minor Street } & \text { ARMENIA }\end{array}$

4/5/2022 Phasing Date:
Computer System I Orientation. North/South Computer system LP| Date: 4/5/2022 Orientation: East / West

$$
31.0
$$

Controller Type EOS |  | Controller Operation |  |
| :--- | :--- | :--- |
| RXR Preempt: | No | FDOT SOP: 10 MOD | Backup Protection: N LPI Location $(\mathrm{Y} / \mathrm{N})$ : Yes

\[
$$
\begin{aligned}
& \text { Crossing Guard Times AM: } \\
& \text { Crossing Guard Times PM: } \\
& \text { Free Time Primary: } \\
& \text { Free Time Secondary: } \\
& \text { Flash Source- (Clomputer or (F)ield: } \\
& \text { Flash Times Primary: } \\
& \text { Flash Times Secondary } \\
& \text { CNA } \emptyset \text { 's } \quad \varnothing 2, \emptyset 6 \\
& \hline
\end{aligned}
$$

\] | 8 |
| :---: |
| SB |
| 10 |
| 3.0 |
| 4.4 |
| 2 |
| 40 | | 55 |
| :---: |
| 7 |

 Fire Preempt: Bridge Preempt: No
Transit Preempt: False Shop Number: 1514 Drop:
$\qquad$

## 7/2/2010

Phasing Date:

$$
\begin{array}{|c|c|c|c|c|c|}
\hline 1 & 2 & 3 & 4 & 5 & 6 \\
\hline E B L T & \text { WB } & \mathrm{SB} L T & \mathrm{NB} & \text { WBLT } & E B \\
\hline \hline
\end{array}
$$

25

 Cll

 \begin{tabular}{|l||}
\hline Controller Phase Number <br>
\hline Direction <br>
\hline Minimum Green <br>
\hline Vehicle Extention <br>
\hline Yellow Clr/Alt Clr <br>
\hline Red CIr/Alt Red Clr <br>
\hline Max Green I <br>
\hline Max Green II <br>
\hline Walk <br>
\hline Walk - XGuard <br>
\hline FDW <br>
\hline FDW - XGuard <br>
\hline Detector Memory <br>
\hline Phase Recall <br>
\hline Ped Recall <br>
\hline Flash Operation <br>
\hline \hline

 

\hline 10 \& 5 <br>
\hline 3.0 \& 3.0 <br>
\hline

 

\hline 4.4 \& 4.9 <br>
\hline

 

\hline 2 \& 2 <br>
\hline 40 \& 15 <br>
\hline

 

\hline 55 \& 25 <br>
\hline 7 \& <br>
\hline
\end{tabular}

1

| 4.9 | 4.9 | 4.4 |
| :---: | :---: | :---: |
| 2 | 2 | 2 |
| 25 | 80 | 20 |
| 30 | 115 | 25 |
|  | 7 |  |
|  |  |  |
|  | 28 |  |
|  |  |  |
| ON | -- | -- |
| -- | MAX | -- |
| -- | ON | - |
| RED | YEL | -- |

$$
\begin{array}{|c|}
\hline 4.9 \\
\hline 2 \\
\hline 90 \\
\hline \hline
\end{array}
$$

$$
\begin{array}{|c|}
\hline \hline 5 \\
\hline 3.0 \\
\hline 4.4 \\
\hline 2 \\
\hline 20 \\
\hline \hline
\end{array}
$$ Date: 4/5/22 Review By: 7 RHC Date04/05/2022Approved By N/A/A Date:4/7/2022



Coordination Pattern Page
Patterns 1-16 Phases 1-8
Major Street: HILLSBOROUGH


Coord Date: 5/21/2021

| EBLT | WB | SB LT | NB | WBLT | EB | NB LT | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |

 Direction:


Ver. $E$
4/5/2022
Coord Date:
웅


| Direction: | EBLT | WB | SB LT | NB | WBLT | EB | NB LT |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ( | SB |  |  |  |  |  |  | |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- |
| Ø Number: | 1 | 2 | 3 | 4 |


| 42 | 80 | 18 | 60 | 42 | 80 | 18 | 60 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |




Patterns 33-48, Phases 1-8 Section Id: 609 S


Major Street: HILLSBOROUGH

## Minor Street: ARMENIA


Sequence

## 



## Plan, SOP and Signal Heads Page



Controller Type Cobalt - EOS
Computer System Cent
Last Date Sent 11/7/2014

oller Operation
FDOT SOP: 7 MOD
Backup Protection: $N$
LPI Location $(\mathrm{Y} / \mathrm{N}): Y$
LPI Date: $5 / 21 / 2021$ LPI Date: 5/21/2021

## 1809

## Drop:

Shop Number:
Phasing Date: 7/2/2010
Orientation: East / West
Orientation: North / South Controller Timings (seconds)
Major Street HILLSBOROUGH

## 4/6/2022

Timing Date:

## SECID: 611

611 Timing Date:

## $\begin{array}{ll}\text { Major Street } & \text { HILLSBOROUGH } \\ \text { Minor Street } & \text { ROME }\end{array}$


Controller Phase Number
Controller Phase Number

| 1 | 2 |  |
| :--- | :---: | :---: |
| Direction | EBLT | WB |


| 5 | 15 |  |
| :---: | :---: | :---: |
| 3.0 | 3.0 |  |
| 4.8 | 4.8 |  | | 1 | 2 |  | 4 | 5 |
| :---: | :---: | :--- | :---: | :---: |
| EBLT | WB |  | NB | WBLT |
| 5 | 15 |  | 10 | 5 |

Transit Preempt: False
Crossing Guard Times AM:
Crossing Guard Times PM:
Free Time Primary:
Free Time Secondary:
Flash Times Primary:
Flash Times Secondary
CNA $\varnothing$ 's $\quad \varnothing 2, \phi$

Flash Source- (C)omputer or (F)ield:

| $\infty$ | $\infty$ |
| :--- | :--- |


| 8 |
| :---: |
| 5 |
| 10 |
| 4.0 |
| 3.7 |
| 2.6 |
| 65 |

$\stackrel{4}{6}$ 7
28
T 1 $\cdots$
--$\xrightarrow{\square}$

| Cabinet Load Switch Assignments |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LS1: | 01 | LS2: | 02 | L53: | L.54: | 04 | LS5: | $\square 5$ | LS6: | 06 | LS7: |  | L.58: | 08 |
| LS9: |  | LS10: |  | LS11: | LS12: |  | L513: | P2 | LS14: | P4 | LS15: | P6 | LS16: | P8 |

*FDOT Timing Project 2014 - Lead/Lag by input and TOD.*
Albeck Gerken, Inc. timings in effect -5/21/2021
New cabinet \& EOS controller 4/2022
LF 35 Sec $2 / 4 / 6 / 8$


Major Street: HILLSBOROUGH
Minor Street: ROME

| NB | WBLT | $E B$ |  | SB <br> 4 |
| :---: | :---: | :---: | :---: | :---: |
|  | 6 |  | 8 |  |



Ver. E
Print Date: $4 / 6 / 2022$
Coord Date: 4/6/2022
71
611 Record Number:
Section Id:

Offset





## Major Street: HILLSBOROUGH

Coord Pattern Page
Ver. $E$
Coord Date:
Coord Structure Table Record \# 71

| Direction: | EBLT | WB |  | NB | WBLT | EB |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\varnothing$ Number: | 1 | 2 |  | 4 | 5 | 6 |  |





| Signal ID: | 0612 |
| ---: | :--- |
| Major Street: | Hillsborough Ave |
| Minor Street: | Lee PI |

Day Plans

| Monday-Thursday |  |  |  |
| :---: | :---: | :---: | :---: |
| Day Plan 1 |  |  |  |
| $\mathbf{H r}$ | Min | Patt | Cycl |
| 00 | 00 | 7 | 150 |
| 05 | 30 | 1 | 210 |
| 09 | 30 | 2 | 180 |
| 11 | 15 | 3 | 180 |
| 13 | 30 | 4 | 180 |
| 14 | 00 | 5 | 200 |
| 18 | 30 | 6 | 150 |
| 21 | 30 | 7 | 150 |
|  |  |  |  |
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| Friday |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Day Plan 2 |  |  |  |  |
| Hr | Min | Patt | Cycl |  |
| 00 | 00 | 7 | 150 |  |
| 05 | 30 | 1 | 210 |  |
| 09 | 30 | 2 | 180 |  |
| 11 | 15 | 3 | 180 |  |
| 13 | 30 | 4 | 180 |  |
| 14 | 00 | 5 | 200 |  |
| 19 | 00 | 6 | 150 |  |
| 21 | 30 | 7 | 150 |  |
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| Saturday |  |  |  |
| :---: | :---: | :---: | :---: |
| Day Plan 3 |  |  |  |
| $\mathbf{H r}$ | Min | Patt | $\mathbf{C y c l}$ |
| 00 | 00 | 7 | 150 |
| 08 | 00 | 8 | 150 |
| 10 | 00 | 9 | 210 |
| 19 | 00 | 10 | 150 |
| 22 | 30 | 7 | 150 |
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| Sunday |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Day Plan 4 |  |  |  |  |
| Hr | Min | Patt | Cycl |  |
| 00 | 00 | 7 | 150 |  |
| 09 | 30 | 8 | 150 |  |
| 11 | 00 | 9 | 210 |  |
| 16 | 00 | 10 | 150 |  |
| 20 | 30 | 7 | 150 |  |
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| Day Plan 5 |  |  |  |  |
| :--- | :--- | :--- | :--- | :---: |
| $\mathbf{H r}$ | Min | Patt | Cycl |  |
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| Patt | Force | Detector | Timing | Coord | Alt Time Table Max Values (Seconds) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Patt | Mode | Plan | Plan | Max Plan | 01 | 02 | 03 | Ø4 | 05 | 06 | $\boxed{\square} 7$ | 08 | 09 | 010 | 011 | 012 | 013 | 014 | 015 | 016 |
| 1 | Float |  |  | MAXİNH |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 | Float |  |  | MAXINH |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | Float |  |  | MAXINH |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | Float |  |  | MAXINH |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | Float |  |  | MAXINH |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6 | Float |  |  | MAXINH |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | Float |  |  | MAXINH |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 | Float |  |  | MAXINH |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9 | Float |  |  | MAXINH |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | Float |  |  | MAXINH |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
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## INTERSECTION ANALYSIS

HCM 6th Signalized Intersection Summary
1：Armenia Ave \＆Hillsborough Ave

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | 9 | 坐平矣 |  | ${ }^{7} 1$ | 平兆家 |  | \％ | 脊 |  | 7 | 个 ${ }^{\text {a }}$ |  |
| Traffic Volume（veh／h） | 158 | 1654 | 183 | 201 | 1953 | 52 | 181 | 278 | 105 | 221 | 569 | 88 |
| Future Volume（veh／h） | 158 | 1654 | 183 | 201 | 1953 | 52 | 181 | 278 | 105 | 221 | 569 | 88 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1811 | 1856 | 1870 | 1841 | 1737 | 1885 | 1870 | 1885 | 1856 | 1885 | 1885 |
| Adj Flow Rate，veh／h | 165 | 1723 | 172 | 209 | 2034 | 49 | 189 | 290 | 98 | 230 | 593 | 83 |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Percent Heavy Veh，\％ | 2 | 6 | 3 | 2 | 4 | 11 | 1 | 2 | 1 | 3 | 1 |  |
| Cap，veh／h | 183 | 2360 | 235 | 216 | 2654 | 64 | 214 | 468 | 155 | 313 | 635 | 89 |
| Arrive On Green | 0.05 | 0.52 | 0.52 | 0.02 | 0.17 | 0.17 | 0.09 | 0.18 | 0.18 | 0.12 | 0.20 | 0.20 |
| Sat Flow，veh／h | 3456 | 4570 | 455 | 3456 | 5048 | 121 | 1795 | 2623 | 868 | 1767 | 3156 | 441 |
| Grp Volume（v），veh／h | 165 | 1241 | 654 | 209 | 1349 | 734 | 189 | 195 | 193 | 230 | 336 | 340 |
| Grp Sat Flow（s），veh／h／ln | 1728 | 1648 | 1729 | 1728 | 1675 | 1819 | 1795 | 1777 | 1714 | 1767 | 1791 | 1806 |
| Q Serve（g＿s），s | 10.0 | 61.4 | 61.8 | 12.7 | 80.6 | 80.8 | 18.0 | 21.2 | 22.0 | 22.1 | 38.7 | 38.9 |
| Cycle Q Clear（g＿c），s | 10.0 | 61.4 | 61.8 | 12.7 | 80.6 | 80.8 | 18.0 | 21.2 | 22.0 | 22.1 | 38.7 | 38.9 |
| Prop In Lane | 1.00 |  | 0.26 | 1.00 |  | 0.07 | 1.00 |  | 0.51 | 1.00 |  | 0.24 |
| Lane Grp Cap（c），veh／h | 183 | 1702 | 893 | 216 | 1762 | 956 | 214 | 317 | 306 | 313 | 361 | 364 |
| VIC Ratio（X） | 0.90 | 0.73 | 0.73 | 0.97 | 0.77 | 0.77 | 0.88 | 0.61 | 0.63 | 0.74 | 0.93 | 0.94 |
| Avail Cap（c＿a），veh／h | 183 | 1702 | 893 | 216 | 1762 | 956 | 214 | 317 | 306 | 356 | 380 | 384 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 0.33 | 0.33 | 0.33 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（I） | 1.00 | 1.00 | 1.00 | 0.41 | 0.41 | 0.41 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 98.9 | 39.4 | 39.5 | 102.6 | 74.5 | 74.5 | 65.5 | 79.6 | 79.9 | 61.3 | 82.4 | 82.5 |
| Incr Delay（d2），s／veh | 40.5 | 2.8 | 5.3 | 31.5 | 1.4 | 2.5 | 32.0 | 3.5 | 4.2 | 6.7 | 28.8 | 29.3 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 5.5 | 25.2 | 27.2 | 6.9 | 36.9 | 40.5 | 10.2 | 10.0 | 10.1 | 10.5 | 20.8 | 21.1 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 139.4 | 42.2 | 44.8 | 134.1 | 75.8 | 77.0 | 97.5 | 83.1 | 84.1 | 68.0 | 111.2 | 111.9 |
| LnGrp LOS | F | D | D | F | E | E | F | F | F | E | F | F |
| Approach Vol，veh／h |  | 2060 |  |  | 2292 |  |  | 577 |  |  | 906 |  |
| Approach Delay，s／veh |  | 50.8 |  |  | 81.5 |  |  | 88.1 |  |  | 100.5 |  |
| Approach LOS |  | D |  |  | F |  |  | F |  |  | F |  |
| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Phs Duration（ $G+Y+R \mathrm{c}$ ），$s$ | 18.0 | 117.3 | 30.8 | 43.9 | 20.0 | 115.3 | 26.0 | 48.7 |  |  |  |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ），s | 6.9 | 6.9 | 6.4 | 6.4 | 6.9 | 6.9 | 6.4 | 6.4 |  |  |  |  |
| Max Green Setting（Gmax），s | 11.1 | 108.1 | 29.6 | 34.6 | 13.1 | 106.1 | 19.6 | 44.6 |  |  |  |  |
| Max Q Clear Time（g＿c＋11），s | 12.0 | 82.8 | 24.1 | 24.0 | 14.7 | 63.8 | 20.0 | 40.9 |  |  |  |  |
| Green Ext Time（p＿c），s | 0.0 | 16.3 | 0.3 | 1.5 | 0.0 | 19.1 | 0.0 | 1.4 |  |  |  |  |

Intersection Summary
HCM 6th Ctri Delay
74.3

HCM 6th LOS
E

HCM 6th Signalized Intersection Summary
1：Armenia Ave \＆Hillsborough Ave

|  | 4 | $\rightarrow$ | $\checkmark$ | $\downarrow$ | 4 | 4 | 4 | $\dagger$ | 7 | $\pm$ | $\dagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 4 | 平車 |  | ${ }^{7 \%}$ | 釉令 |  | ${ }^{7}$ | 94 |  | \％ | 車食 |  |
| Traffic Volume（veh／h） | 432 | 2028 | 176 | 122 | 1832 | 142 | 215 | 606 | 108 | 131 | 345 | 150 |
| Future Volume（veh／h） | 432 | 2028 | 176 | 122 | 1832 | 142 | 215 | 606 | 108 | 131 | 345 | 150 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1885 | 1870 | 1885 | 1856 | 1841 | 1841 | 1885 | 1870 | 1870 | 1856 | 1885 | 1885 |
| Adj Flow Rate，veh／h | 441 | 2069 | 162 | 124 | 1869 | 131 | 219 | 618 | 99 | 134 | 352 | 138 |
| Peak Hour Factor | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Percent Heavy Veh，\％ | 1 | 2 | 1 | 3 | 4 | 4 | 1 | 2 | 2 | 3 | 1 | 1 |
| Cap，veh／h | 420 | 2590 | 201 | 157 | 2212 | 155 | 257 | 666 | 107 | 170 | 486 | 187 |
| Arrive On Green | 0.12 | 0.54 | 0.54 | 0.09 | 0.92 | 0.92 | 0.09 | 0.22 | 0.22 | 0.07 | 0.19 | 0.19 |
| Sat Flow，veh／h | 3483 | 4831 | 376 | 3428 | 4795 | 335 | 1795 | 3068 | 491 | 1767 | 2526 | 974 |
| Grp Volume（v），veh／h | 441 | 1453 | 778 | 124 | 1304 | 696 | 219 | 357 | 360 | 134 | 248 | 242 |
| Grp Sat Flow（s），veh／h／in | 1742 | 1702 | 1803 | 1714 | 1675 | 1780 | 1795 | 1777 | 1782 | 1767 | 1791 | 1710 |
| Q Serve（g＿s），s | 24.1 | 69.1 | 70.4 | 7.1 | 27.2 | 27.8 | 18.6 | 39.4 | 39.6 | 12.1 | 25.9 | 26.7 |
| Cycle Q Clear（g＿c），s | 24.1 | 69.1 | 70.4 | 7.1 | 27.2 | 27.8 | 18.6 | 39.4 | 39.6 | 12.1 | 25.9 | 26.7 |
| Prop In Lane | 1.00 |  | 0.21 | 1.00 |  | 0.19 | 1.00 |  | 0.28 | 1.00 |  | 0.57 |
| Lane Grp Cap（c），veh／h | 420 | 1825 | 966 | 157 | 1545 | 821 | 257 | 386 | 387 | 170 | 344 | 329 |
| V／C Ratio（X） | 1.05 | 0.80 | 0.80 | 0.79 | 0.84 | 0.85 | 0.85 | 0.93 | 0.93 | 0.79 | 0.72 | 0.74 |
| Avail Cap（c＿a），veh／h | 420 | 1825 | 966 | 207 | 1545 | 821 | 257 | 414 | 415 | 170 | 373 | 356 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 0.43 | 0.43 | 0.43 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 87.9 | 37.6 | 37.9 | 89.9 | 5.2 | 5.2 | 61.7 | 76.7 | 76.8 | 62.7 | 75.7 | 76.0 |
| Incr Delay（d2），s／veh | 57.9 | 3.7 | 7.1 | 6.4 | 2.6 | 4.9 | 23.1 | 25.8 | 26.4 | 21.3 | 6.1 | 7.2 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 14.2 | 29.1 | 32.3 | 3.2 | 3.2 | 3.9 | 10.7 | 20.7 | 20.9 | 6.5 | 12.5 | 12.4 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 145.8 | 41.3 | 45.0 | 96.3 | 7.8 | 10.1 | 84.8 | 102.5 | 103.1 | 84.0 | 81.8 | 83.2 |
| LnGrp LOS | F | D | D | F | A | B | F | F | F | F | F | F |
| Approach Vol，veh／h |  | 2672 |  |  | 2124 |  |  | 936 |  |  | 624 |  |
| Approach Delay，s／veh |  | 59.6 |  |  | 13.8 |  |  | 98.6 |  |  | 82.8 |  |
| Approach LOS |  | E |  |  | B |  |  | F |  |  | F |  |
| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Phs Duration（ $G+Y+R \mathrm{c}$ ），$s$ | 31.0 | 99.2 | 20.0 | 49.8 | 16.1 | 114.1 | 25.0 | 44.8 |  |  |  |  |
| Change Period（ $Y+R \mathrm{c}$ ）， s | 6.9 | 6.9 | 6.4 | 6.4 | 6.9 | 6.9 | 6.4 | 6.4 |  |  |  |  |
| Max Green Setting（Gmax），s | 24.1 | 89.1 | 13.6 | 46.6 | 12.1 | 101.1 | 18.6 | 41.6 |  |  |  |  |
| Max Q Clear Time（g＿c＋11），s | 26.1 | 29.8 | 14.1 | 41.6 | 9.1 | 72.4 | 20.6 | 28.7 |  |  |  |  |
| Green Ext Time（p＿c），s | 0.0 | 23.6 | 0.0 | 1.9 | 0.1 | 19.2 | 0.0 | 2.3 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 52.3 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | D |  |  |  |  |  |  |  |  |  |

HCM 6th Signalized Intersection Summary
1: Armenia Ave \& Hillsborough Ave

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | 17 |  | 7 | Yi | ¢444 | 7 | \% | 車 |  | 7 | 仿 |  |
| Traffic Volume (veh/h) | 158 | 1654 | 183 | 201 | 1953 | 52 | 181 | 278 | 105 | 221 | 569 | 88 |
| Future Volume (veh/h) | 158 | 1654 | 183 | 201 | 1953 | 52 | 181 | 278 | 105 | 221 | 569 | 88 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1811 | 1856 | 1870 | 1841 | 1737 | 1885 | 1870 | 1885 | 1856 | 1885 | 1885 |
| Adj Flow Rate, veh/h | 165 | 1723 | 134 | 209 | 2034 | 37 | 189 | 290 | 76 | 230 | 593 | 64 |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Percent Heavy Veh, \% | 2 | 6 | 3 | 2 | 4 | 11 | 1 | 2 | 1 | 3 | 1 |  |
| Cap, veh/h | 196 | 2558 | 814 | 232 | 2652 | 777 | 215 | 481 | 124 | 316 | 637 | 69 |
| Arrive On Green | 0.06 | 0.52 | 0.52 | 0.04 | 0.35 | 0.35 | 0.09 | 0.17 | 0.17 | 0.12 | 0.20 | 0.20 |
| Sat Flow, veh/h | 3456 | 4944 | 1572 | 3456 | 5025 | 1472 | 1795 | 2797 | 720 | 1767 | 3262 | 351 |
| Grp Volume(v), veh/h | 165 | 1723 | 134 | 209 | 2034 | 37 | 189 | 182 | 184 | 230 | 325 | 332 |
| Grp Sat Flow(s),veh/h/n | 1728 | 1648 | 1572 | 1728 | 1675 | 1472 | 1795 | 1777 | 1741 | 1767 | 1791 | 1822 |
| Q Serve(g_s), s | 9.9 | 54.2 | 9.4 | 12.6 | 75.4 | 3.5 | 18.2 | 19.9 | 20.5 | 22.3 | 37.5 | 37.6 |
| Cycle Q Clear (g_c), s | 9.9 | 54.2 | 9.4 | 12.6 | 75.4 | 3.5 | 18.2 | 19.9 | 20.5 | 22.3 | 37.5 | 37.6 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.41 | 1.00 |  | 0.19 |
| Lane Grp Cap(c), veh/h | 196 | 2558 | 814 | 232 | 2652 | 777 | 215 | 305 | 299 | 316 | 350 | 356 |
| V/C Ratio(X) | 0.84 | 0.67 | 0.16 | 0.90 | 0.77 | 0.05 | 0.88 | 0.60 | 0.61 | 0.73 | 0.93 | 0.93 |
| Avail Cap(c_a), veh/h | 199 | 2558 | 814 | 232 | 2652 | 777 | 215 | 305 | 299 | 358 | 372 | 378 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 0.67 | 0.67 | 0.67 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.34 | 0.34 | 0.34 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 98.1 | 37.5 | 26.7 | 99.6 | 56.4 | 33.2 | 66.4 | 80.3 | 80.5 | 62.0 | 83.0 | 83.1 |
| Incr Delay (d2), s/veh | 25.9 | 1.4 | 0.4 | 15.1 | 0.8 | 0.0 | 31.7 | 3.2 | 3.7 | 6.4 | 28.5 | 28.9 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ $(50 \%)$,veh/ln | 5.2 | 22.0 | 3.7 | 6.3 | 33.0 | 1.3 | 10.2 | 9.4 | 9.5 | 10.6 | 20.1 | 20.5 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay (d), s/veh | 123.9 | 39.0 | 27.2 | 114.7 | 57.2 | 33.2 | 98.1 | 83.4 | 84.2 | 68.4 | 111.6 | 112.0 |
| LnGrp LOS | F | D | C | F | E | C | F | F | F | E | F | F |
| Approach Vol, veh/h |  | 2022 |  |  | 2280 |  |  | 555 |  |  | 887 |  |
| Approach Delay, s/veh |  | 45.1 |  |  | 62.1 |  |  | 88.7 |  |  | 100.5 |  |
| Approach LOS |  | D |  |  | E |  |  | F |  |  | F |  |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Phs Duration ( $G+Y+R c$ ), $s$ | 18.8 | 117.7 | 31.0 | 42.5 | 21.0 | 115.6 | 26.0 | 47.4 |  |  |  |  |
| Change Period ( $Y+R \mathrm{c}$ ), $s$ | 6.9 | 6.9 | 6.4 | 6.4 | 6.9 | 6.9 | 6.4 | 6.4 |  |  |  |  |
| Max Green Setting (Gmax), s | 12.1 | 108.1 | 29.6 | 33.6 | 14.1 | 106.1 | 19.6 | 43.6 |  |  |  |  |
| Max Q Clear Time (g_ct1), s | 11.9 | 77.4 | 24.3 | 22.5 | 14.6 | 56.2 | 20.2 | 39.6 |  |  |  |  |
| Green Ext Time (p_c), $s$ | 0.0 | 19.0 | 0.3 | 1.5 | 0.0 | 19.5 | 0.0 | 1.4 |  |  |  |  |

Intersection Summary

| HCM 6th CtrI Delay | 64.6 |
| :--- | ---: |
| HCM 6th LOS | E |

HCM 6th Signalized Intersection Summary
1：Armenia Ave \＆Hillsborough Ave

|  | 4 | $\rightarrow$ | \％ | 7 | 4 | 4 | 4 | 4 | 7 | ＊ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 71 | 个个4 | \％ | 4 | 㑣4 | 「 | 1 | 个㐱 |  | 7 | 个官 |  |
| Traffic Volume（veh／h） | 432 | 2028 | 176 | 122 | 1832 | 142 | 215 | 606 | 108 | 131 | 345 | 150 |
| Future Volume（veh／h） | 432 | 2028 | 176 | 122 | 1832 | 142 | 215 | 606 | 108 | 131 | 345 | 150 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1885 | 1870 | 1885 | 1856 | 1841 | 1841 | 1885 | 1870 | 1870 | 1856 | 1885 | 1885 |
| Adj Flow Rate，veh／h | 441 | 2069 | 126 | 124 | 1869 | 101 | 219 | 618 | 99 | 134 | 352 | 138 |
| Peak Hour Factor | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Percent Heavy Veh，\％ | 1 | 2 | 1 | 3 | 4 | 4 | 1 | 2 | 2 | 3 | 1 | 1 |
| Cap，veh／h | 472 | 2757 | 863 | 158 | 2265 | 703 | 252 | 653 | 104 | 166 | 475 | 183 |
| Arrive On Green | 0.14 | 0.54 | 0.54 | 0.09 | 0.90 | 0.90 | 0.09 | 0.21 | 0.21 | 0.07 | 0.19 | 0.19 |
| Sat Flow，veh／h | 3483 | 5106 | 1598 | 3428 | 5025 | 1560 | 1795 | 3068 | 491 | 1767 | 2526 | 974 |
| Grp Volume（v），veh／h | 441 | 2069 | 126 | 124 | 1869 | 101 | 219 | 357 | 360 | 134 | 248 | 242 |
| Grp Sat Flow（s），veh／h／ln | 1742 | 1702 | 1598 | 1714 | 1675 | 1560 | 1795 | 1777 | 1782 | 1767 | 1791 | 1710 |
| Q Serve（g＿s），s | 25.1 | 62.7 | 7.9 | 7.1 | 28.6 | 1.5 | 18.6 | 39.6 | 39.8 | 12.2 | 26.1 | 26.8 |
| Cycle Q Clear（g＿c），s | 25.1 | 62.7 | 7.9 | 7.1 | 28.6 | 1.5 | 18.6 | 39.6 | 39.8 | 12.2 | 26.1 | 26.8 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.28 | 1.00 |  | 0.57 |
| Lane Grp Cap（c），veh／h | 472 | 2757 | 863 | 158 | 2265 | 703 | 252 | 378 | 379 | 166 | 336 | 321 |
| V／C Ratio（X） | 0.94 | 0.75 | 0.15 | 0.78 | 0.83 | 0.14 | 0.87 | 0.94 | 0.95 | 0.81 | 0.74 | 0.75 |
| Avail Cap（c＿a），veh／h | 472 | 2757 | 863 | 259 | 2265 | 703 | 252 | 387 | 388 | 166 | 346 | 330 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（I） | 1.00 | 1.00 | 1.00 | 0.39 | 0.39 | 0.39 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 85.6 | 35.6 | 23.0 | 89.8 | 6.8 | 5.5 | 62.6 | 77.6 | 77.6 | 63.3 | 76.5 | 76.8 |
| Incr Delay（d2），s／veh | 26.1 | 1.9 | 0.4 | 3.4 | 1.4 | 0.2 | 26.0 | 31.5 | 32.2 | 24.4 | 7.8 | 9.2 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 12.9 | 26.0 | 3.1 | 3.1 | 3.5 | 0.5 | 10.9 | 21.4 | 21.6 | 6.6 | 12.7 | 12.6 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 111.7 | 37.5 | 23.3 | 93.2 | 8.3 | 5.6 | 88.6 | 109.1 | 109.8 | 87.8 | 84.4 | 86.1 |
| LnGrp LOS | F | D | C | F | A | A | F | F | F | F | F | F |
| Approach Vol，veh／h |  | 2636 |  |  | 2094 |  |  | 936 |  |  | 624 |  |
| Approach Delay，s／veh |  | 49.2 |  |  | 13.2 |  |  | 104.6 |  |  | 85.8 |  |
| Approach LOS |  | D |  |  | B |  |  | F |  |  | F |  |
| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Phs Duration（ $G+Y+R \mathrm{c}$ ），$s$ | 34.0 | 97.1 | 20.0 | 49.0 | 16.1 | 114.9 | 25.0 | 44.0 |  |  |  |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ），s | 6.9 | 6.9 | 6.4 | 6.4 | 6.9 | 6.9 | 6.4 | 6.4 |  |  |  |  |
| Max Green Setting（Gmax），s | 27.1 | 89.1 | 13.6 | 43.6 | 15.1 | 101.1 | 18.6 | 38.6 |  |  |  |  |
| Max Q Clear Time（g＿c＋11），s | 27.1 | 30.6 | 14.2 | 41.8 | 9.1 | 64.7 | 20.6 | 28.8 |  |  |  |  |
| Green Ext Time（p＿c），s | 0.0 | 23.2 | 0.0 | 0.8 | 0.2 | 22.0 | 0.0 | 1.9 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 49.1 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | D |  |  |  |  |  |  |  |  |  |

HCM 6th Signalized Intersection Summary
1：Armenia Ave \＆Hillsborough Ave

|  | 4 | $\rightarrow$ | $\cdots$ | 7 | 4 | 4 | 4 | 9 | $p$ | $t$ | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 坐車个 | 7 | 71 | 14¢ㅜ | 7 | ${ }^{7}$ | 4方 |  | \％ | 防 |  |
| Traffic Volume（veh／h） | 158 | 1663 | 183 | 205 | 1982 | 56 | 181 | 278 | 106 | 222 | 569 | 88 |
| Future Volume（veh／h） | 158 | 1663 | 183 | 205 | 1982 | 56 | 181 | 278 | 106 | 222 | 569 | 88 |
| Initial $\mathrm{Q}(\mathrm{Qb})$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1811 | 1856 | 1870 | 1841 | 1737 | 1885 | 1870 | 1885 | 1856 | 1885 | 1885 |
| Adj Flow Rate，veh／h | 165 | 1732 | 134 | 214 | 2065 | 40 | 189 | 290 | 77 | 231 | 593 | 64 |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Percent Heavy Veh，\％ | 2 | 6 | 3 | 2 | 4 | 11 | 1 | 2 | 1 | 3 | 1 | 1 |
| Cap，veh／h | 196 | 2558 | 814 | 232 | 2652 | 777 | 215 | 478 | 125 | 316 | 637 | 69 |
| Arrive On Green | 0.06 | 0.52 | 0.52 | 0.04 | 0.35 | 0.35 | 0.09 | 0.17 | 0.17 | 0.12 | 0.20 | 0.20 |
| Sat Flow，veh／h | 3456 | 4944 | 1572 | 3456 | 5025 | 1472 | 1795 | 2789 | 728 | 1767 | 3262 | 351 |
| Grp Volume（v），veh／h | 165 | 1732 | 134 | 214 | 2065 | 40 | 189 | 183 | 184 | 231 | 325 | 332 |
| Grp Sat Flow（s），veh／h／ln | 1728 | 1648 | 1572 | 1728 | 1675 | 1472 | 1795 | 1777 | 1739 | 1767 | 1791 | 1822 |
| Q Serve（g＿s），s | 9.9 | 54.6 | 9.4 | 13.0 | 77.0 | 3.8 | 18.2 | 20.0 | 20.6 | 22.4 | 37.5 | 37.6 |
| Cycle Q Clear（g＿c），s | 9.9 | 54.6 | 9.4 | 13.0 | 77.0 | 3.8 | 18.2 | 20.0 | 20.6 | 22.4 | 37.5 | 37.6 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.42 | 1.00 |  | 0.19 |
| Lane Grp Cap（c），veh／h | 196 | 2558 | 814 | 232 | 2652 | 777 | 215 | 304 | 298 | 316 | 350 | 356 |
| V／C Ratio（X） | 0.84 | 0.68 | 0.16 | 0.92 | 0.78 | 0.05 | 0.88 | 0.60 | 0.62 | 0.73 | 0.93 | 0.93 |
| Avail Cap（c＿a），veh／h | 199 | 2558 | 814 | 232 | 2652 | 777 | 215 | 304 | 298 | 357 | 372 | 378 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 0.67 | 0.67 | 0.67 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 0.32 | 0.32 | 0.32 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 98.1 | 37.6 | 26.7 | 99.7 | 56.9 | 33.3 | 66.4 | 80.4 | 80.6 | 62.0 | 83.0 | 83.1 |
| Incr Delay（d2），s／veh | 25.9 | 1.5 | 0.4 | 17.3 | 0.8 | 0.0 | 31.7 | 3.3 | 3.8 | 6.6 | 28.5 | 28.9 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 5.2 | 22.2 | 3.7 | 6.5 | 33.7 | 1.4 | 10.2 | 9.5 | 9.6 | 10.7 | 20.1 | 20.5 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 123.9 | 39.1 | 27.2 | 117.0 | 57.7 | 33.3 | 98.1 | 83.6 | 84.5 | 68.6 | 111.6 | 112.0 |
| LnGrp LOS | F | D | C | F | E | C | F | F | F | E | F | F |
| Approach Vol，veh／h |  | 2031 |  |  | 2319 |  |  | 556 |  |  | 888 |  |
| Approach Delay，s／veh |  | 45.2 |  |  | 62.7 |  |  | 88.8 |  |  | 100.5 |  |
| Approach LOS |  | D |  |  | E |  |  | F |  |  | F |  |
| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Phs Duration（ $G+Y+R \mathrm{c}$ ），$s$ | 18.8 | 117.7 | 31.1 | 42.4 | 21.0 | 115.6 | 26.0 | 47.4 |  |  |  |  |
| Change Period（ $Y+R \mathrm{c}$ ），s | 6.9 | 6.9 | 6.4 | 6.4 | 6.9 | 6.9 | 6.4 | 6.4 |  |  |  |  |
| Max Green Setting（Gmax），s | 12.1 | 108.1 | 29.6 | 33.6 | 14.1 | 106.1 | 19.6 | 43.6 |  |  |  |  |
| Max Q Clear Time（g＿c＋11），s | 11.9 | 79.0 | 24.4 | 22.6 | 15.0 | 56.6 | 20.2 | 39.6 |  |  |  |  |
| Green Ext Time（p＿c），s | 0.0 | 18.7 | 0.3 | 1.5 | 0.0 | 19.6 | 0.0 | 1.4 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 64.9 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | E |  |  |  |  |  |  |  |  |  |

HCM 6th Signalized Intersection Summary
1: Armenia Ave \& Hillsborough Ave

|  | $\rightarrow$ |  | $\square$ | 7 | $\nleftarrow$ | 4 | 4 | $\dagger$ | \% | , | $\downarrow$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 4 |  | 7 | ${ }^{717}$ | 44个 | 7 | 7 | 4\% |  | 7 | 性 |  |
| Traffic Volume (veh/h) | 432 | 2054 | 176 | 124 | 1850 | 144 | 215 | 606 | 112 | 135 | 345 | 150 |
| Future Volume (veh/h) | 432 | 2054 | 176 | 124 | 1850 | 144 | 215 | 606 | 112 | 135 | 345 | 150 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1885 | 1870 | 1885 | 1856 | 1841 | 1841 | 1885 | 1870 | 1870 | 1856 | 1885 | 1885 |
| Adj Flow Rate, veh/h | 441 | 2096 | 126 | 127 | 1888 | 102 | 219 | 618 | 102 | 138 | 352 | 138 |
| Peak Hour Factor | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Percent Heavy Veh, \% | 1 | 2 | 1 | 3 | 4 | 4 | 1 | 2 | 2 | 3 | 1 | 1 |
| Cap, veh/h | 472 | 2750 | 860 | 161 | 2262 | 702 | 253 | 652 | 107 | 166 | 476 | 184 |
| Arrive On Green | 0.14 | 0.54 | 0.54 | 0.09 | 0.90 | 0.90 | 0.09 | 0.21 | 0.21 | 0.07 | 0.19 | 0.19 |
| Sat Flow, veh/h | 3483 | 5106 | 1598 | 3428 | 5025 | 1560 | 1795 | 3054 | 503 | 1767 | 2526 | 974 |
| Grp Volume(v), veh/h | 441 | 2096 | 126 | 127 | 1888 | 102 | 219 | 359 | 361 | 138 | 248 | 242 |
| Grp Sat Flow(s),veh/h/ln | 1742 | 1702 | 1598 | 1714 | 1675 | 1560 | 1795 | 1777 | 1780 | 1767 | 1791 | 1710 |
| Q Serve(g_s), s | 25.1 | 64.3 | 7.9 | 7.2 | 30.2 | 1.5 | 18.6 | 39.8 | 40.0 | 12.6 | 26.1 | 26.8 |
| Cycle Q Clear(g_c), s | 25.1 | 64.3 | 7.9 | 7.2 | 30.2 | 1.5 | 18.6 | 39.8 | 40.0 | 12.6 | 26.1 | 26.8 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.28 | 1.00 |  | 0.57 |
| Lane Grp Cap(c), veh/h | 472 | 2750 | 860 | 161 | 2262 | 702 | 253 | 379 | 380 | 166 | 338 | 322 |
| V/C Ratio(X) | 0.94 | 0.76 | 0.15 | 0.79 | 0.83 | 0.15 | 0.87 | 0.95 | 0.95 | 0.83 | 0.73 | 0.75 |
| Avail Cap(c_a), veh/h | 472 | 2750 | 860 | 259 | 2262 | 702 | 253 | 387 | 388 | 166 | 346 | 330 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 0.37 | 0.37 | 0.37 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 85.6 | 36.1 | 23.1 | 89.6 | 7.0 | 5.6 | 62.5 | 77.5 | 77.6 | 63.4 | 76.4 | 76.7 |
| Incr Delay (d2), s/veh | 26.1 | 2.1 | 0.4 | 3.2 | 1.5 | 0.2 | 25.5 | 32.0 | 32.6 | 28.6 | 7.7 | 9.1 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%), veh/ln | 12.9 | 26.7 | 3.1 | 3.2 | 3.6 | 0.5 | 10.9 | 21.5 | 21.7 | 7.0 | 12.7 | 12.6 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGro Delay(d),s/veh | 111.7 | 38.2 | 23.5 | 92.9 | 8.5 | 5.7 | 88.0 | 109.5 | 110.2 | 92.0 | 84.1 | 85.8 |
| LnGrp LOS | F | D | C | F | A | A | F | F | F | F | F | F |
| Approach Vol, veh/h |  | 2663 |  |  | 2117 |  |  | 939 |  |  | 628 |  |
| Approach Delay, s/veh |  | 49.7 |  |  | 13.4 |  |  | 104.7 |  |  | 86.5 |  |
| Approach LOS |  | D |  |  | B |  |  | F |  |  | F |  |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Phs Duration ( $G+Y+R \mathrm{c})$, $s$ | 34.0 | 96.9 | 20.0 | 49.1 | 16.3 | 114.6 | 25.0 | 44.1 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 6.9 | 6.9 | 6.4 | 6.4 | 6.9 | 6.9 | 6.4 | 6.4 |  |  |  |  |
| Max Green Setting (Gmax), s | 27.1 | 89.1 | 13.6 | 43.6 | 15.1 | 101.1 | 18.6 | 38.6 |  |  |  |  |
| Max Q Clear Time (g_c+11), s | 27.1 | 32.2 | 14.6 | 42.0 | 9.2 | 66.3 | 20.6 | 28.8 |  |  |  |  |
| Green Ext Time (p_c), s | 0.0 | 23.5 | 0.0 | 0.7 | 0.2 | 21.8 | 0.0 | 1.9 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 49.4 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | D |  |  |  |  |  |  |  |  |  |

HCM 6th Signalized Intersection Summary
2：Rome Ave \＆Hillsborough Ave

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | 7 | 雨 $\hat{5}$ |  | 7 | 44家 |  | 7 | 个 | F | ${ }^{1}$ | F |  |
| Traffic Volume（veh／h） | 123 | 1688 | 190 | 85 | 2035 | 60 | 119 | 161 | 68 | 136 | 243 | 101 |
| Future Volume（veh／h） | 123 | 1688 | 190 | 85 | 2035 | 60 | 119 | 161 | 68 | 136 | 243 | 101 |
| Initial $\mathrm{Q}(\mathrm{Qb})$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1885 | 1826 | 1885 | 1885 | 1841 | 1841 | 1856 | 1870 | 1826 | 1870 | 1870 | 1856 |
| Adj Flow Rate，veh／h | 132 | 1815 | 184 | 91 | 2188 | 59 | 128 | 173 | 51 | 146 | 261 | 98 |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Percent Heavy Veh，\％ | 1 | 5 | 1 | 1 | 4 | 4 | 3 | 2 | 5 | 2 | 2 | 3 |
| Cap，veh／h | 149 | 2634 | 266 | 96 | 2730 | 73 | 134 | 523 | 433 | 273 | 362 | 136 |
| Arrive On Green | 0.03 | 0.19 | 0.19 | 0.11 | 1.00 | 1.00 | 0.28 | 0.28 | 0.28 | 0.28 | 0.28 | 0.28 |
| Sat Flow，veh／h | 1795 | 4601 | 464 | 1795 | 5031 | 135 | 1014 | 1870 | 1547 | 1157 | 1296 | 487 |
| Grp Volume（v），veh／h | 132 | 1309 | 690 | 91 | 1455 | 792 | 128 | 173 | 51 | 146 | 0 | 359 |
| Grp Sat Flow（s），veh／h／ln | 1795 | 1662 | 1742 | 1795 | 1675 | 1816 | 1014 | 1870 | 1547 | 1157 | 0 | 1783 |
| Q Serve（g＿s），s | 15.4 | 77.1 | 77.7 | 10.6 | 0.0 | 0.0 | 20.5 | 15.4 | 5.2 | 24.1 | 0.0 | 38.2 |
| Cycle Q Clear（g＿c），s | 15.4 | 77.1 | 77.7 | 10.6 | 0.0 | 0.0 | 58.7 | 15.4 | 5.2 | 39.5 | 0.0 | 38.2 |
| Prop In Lane | 1.00 |  | 0.27 | 1.00 |  | 0.07 | 1.00 |  | 1.00 | 1.00 |  | 0.27 |
| Lane Grp Cap（c），veh／h | 149 | 1902 | 997 | 96 | 1818 | 986 | 134 | 523 | 433 | 273 | 0 | 498 |
| V／C Ratio（X） | 0.89 | 0.69 | 0.69 | 0.95 | 0.80 | 0.80 | 0.96 | 0.33 | 0.12 | 0.54 | 0.00 | 0.72 |
| Avail Cap（c＿a），veh／h | 164 | 1902 | 997 | 96 | 1818 | 986 | 134 | 523 | 433 | 273 | 0 | 498 |
| HCM Platoon Ratio | 0.33 | 0.33 | 0.33 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 0.54 | 0.54 | 0.54 | 0.78 | 0.78 | 0.78 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay（d），s／veh | 101.1 | 67.7 | 67.9 | 93.5 | 0.0 | 0.0 | 97.0 | 60.1 | 56.4 | 75.7 | 0.0 | 68.2 |
| Incr Delay（d2），s／veh | 23.9 | 1.1 | 2.2 | 65.7 | 3.0 | 5.5 | 65.0 | 0.4 | 0.1 | 2.0 | 0.0 | 5.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 8.5 | 35.0 | 37.2 | 6.4 | 0.8 | 1.5 | 9.5 | 7.5 | 2.1 | 7.4 | 0.0 | 18.3 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 125.0 | 68.8 | 70.1 | 159.2 | 3.0 | 5.5 | 162.0 | 60.4 | 56.5 | 77.8 | 0.0 | 73.3 |
| LnGrp LOS | F | E | E | F | A | A | F | E | E | E | A | E |
| Approach Vol，veh／h |  | 2131 |  |  | 2338 |  |  | 352 |  |  | 505 |  |
| Approach Delay，s／veh |  | 72.7 |  |  | 9.9 |  |  | 96.8 |  |  | 74.6 |  |
| Approach LOS |  | E |  |  | A |  |  | F |  |  | E |  |
| Timer－Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration（ $G+Y+R \mathrm{c}$ ），$s$ | 24.2 | 120.8 |  | 65.0 | 18.0 | 127.0 |  | 65.0 |  |  |  |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ）， s | 6.8 | 6.8 |  | ＊ 6.3 | 6.8 | 6.8 |  | ＊ 6.3 |  |  |  |  |
| Max Green Setting（Gmax），s | 19.2 | 112.2 |  | ＋59 | 11.2 | 120.2 |  | ＊ 59 |  |  |  |  |
| Max Q Clear Time（g＿ct｜1），s | 17.4 | 2.0 |  | 60.7 | 12.6 | 79.7 |  | 41.5 |  |  |  |  |
| Green Ext Time（p＿c），s | 0.0 | 35.4 |  | 0.0 | 0.0 | 20.4 |  | 2.6 |  |  |  |  |

## Intersection Summary

HCM 6th Ctrl Delay 46.9

HCM 6th LOS
D
＊NCM 6 th computational engine requires equal clearance times for the phases crossing the barrier．

HCM 6th Signalized Intersection Summary
2：Rome Ave \＆Hillsborough Ave

|  | 7 | $\rightarrow$ | 7 | 7 | － | 4 | 4 | 4 | \％ | $\downarrow$ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 个性 |  | ${ }^{7}$ | 个慣 |  | \％ | $\uparrow$ | 「 | \％ | $\dagger$ |  |
| Traffic Volume（veh／h） | 238 | 2102 | 95 | 59 | 1908 | 143 | 119 | 298 | 78 | 85 | 143 | 72 |
| Future Volume（veh／h） | 238 | 2102 | 95 | 59 | 1908 | 143 | 119 | 298 | 78 | 85 | 143 | 72 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／n | 1885 | 1870 | 1885 | 1870 | 1841 | 1841 | 1885 | 1885 | 1885 | 1856 | 1856 | 1870 |
| Adj Flow Rate，veh／h | 256 | 2260 | 91 | 63 | 2052 | 138 | 128 | 320 | 75 | 91 | 154 | 69 |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Percent Heavy Veh，\％ | 1 | 2 | 1 | 2 | 4 | 4 | 1 | 1 | 1 | 3 | 3 | 2 |
| Cap，veh／h | 270 | 3032 | 121 | 78 | 2382 | 159 | 207 | 480 | 407 | 137 | 309 | 139 |
| Arrive On Green | 0.30 | 1.00 | 1.00 | 0.09 | 0.99 | 0.99 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 |
| Sat Flow，veh／h | 1795 | 5036 | 202 | 1781 | 4811 | 322 | 1167 | 1885 | 1598 | 981 | 1214 | 544 |
| Grp Volume（v），veh／h | 256 | 1524 | 827 | 63 | 1425 | 765 | 128 | 320 | 75 | 91 | 0 | 223 |
| Grp Sat Flow（s），veh／h／h | 1795 | 1702 | 1834 | 1781 | 1675 | 1783 | 1167 | 1885 | 1598 | 981 | 0 | 1758 |
| Q Serve（g＿s），s | 27.9 | 0.0 | 0.0 | 6.9 | 5.6 | 5.9 | 21.0 | 30.5 | 7.3 | 18.3 | 0.0 | 21.7 |
| Cycle Q Clear（g＿c），s | 27.9 | 0.0 | 0.0 | 6.9 | 5.6 | 5.9 | 42.7 | 30.5 | 7.3 | 48.8 | 0.0 | 21.7 |
| Prop In Lane | 1.00 |  | 0.11 | 1.00 |  | 0.18 | 1.00 |  | 1.00 | 1.00 |  | 0.31 |
| Lane Grp Cap（c），veh／h | 270 | 2050 | 1104 | 78 | 1659 | 883 | 207 | 480 | 407 | 137 | 0 | 448 |
| VIC Ratio（X） | 0.95 | 0.74 | 0.75 | 0.81 | 0.86 | 0.87 | 0.62 | 0.67 | 0.18 | 0.67 | 0.00 | 0.50 |
| Avail Cap（c＿a），veh／h | 298 | 2050 | 1104 | 118 | 1659 | 883 | 211 | 487 | 413 | 140 | 0 | 454 |
| HCM Platoon Ratio | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 0.39 | 0.39 | 0.39 | 0.83 | 0.83 | 0.83 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay（d），s／veh | 69.1 | 0.0 | 0.0 | 90.5 | 0.5 | 0.5 | 81.8 | 66.9 | 58.3 | 88.8 | 0.0 | 63.6 |
| Incr Delay（d2），slveh | 19.8 | 1.0 | 1.9 | 18.6 | 5.1 | 9.5 | 5.2 | 3.4 | 0.2 | 11.0 | 0.0 | 0.9 |
| Initial Q Delay（d3），${ }^{\text {／veh }}$ | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（ $50 \%$ ），veh／ln | 12.8 | 0.3 | 0.6 | 3.5 | 1.5 | 2.7 | 6.7 | 15.3 | 3.1 | 5.1 | 0.0 | 9.9 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 88.9 | 1.0 | 1.9 | 109.1 | 5.6 | 10.0 | 87.0 | 70.2 | 58.5 | 99.8 | 0.0 | 64.4 |
| LnGrp LOS | F | A | A | F | A | A | F | E | E | F | A | E |
| Approach Vol，veh／h |  | 2607 |  |  | 2253 |  |  | 523 |  |  | 314 |  |
| Approach Delay，s／veh |  | 9.9 |  |  | 10.0 |  |  | 72.7 |  |  | 74.7 |  |
| Approach LOS |  | A |  |  | A |  |  | E |  |  | E |  |
| Timer－Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration（ $G+Y+\mathrm{Rc}$ ），s | 36.9 | 105.8 |  | 57.3 | 15.5 | 127.2 |  | 57.3 |  |  |  |  |
| Change Period（ $Y+R \mathrm{c}$ ）， s | 6.8 | 6.8 |  | ＊ 6.3 | 6.8 | 6.8 |  | ＊ 6.3 |  |  |  |  |
| Max Green Setting（Gmax），s | 33.2 | 95.2 |  | ＊52 | 13.2 | 115.2 |  | ＊52 |  |  |  |  |
| Max Q Clear Time（g＿c＋1），s | 29.9 | 7.9 |  | 44.7 | 8.9 | 2.0 |  | 50.8 |  |  |  |  |
| Green Ext Time（p＿c），s | 0.2 | 31.8 |  | 1.6 | 0.0 | 40.0 |  | 0.2 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 19.3 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | B |  |  |  |  |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |

＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．

HCM 6th Signalized Intersection Summary
2: Rome Ave \& Hillsborough Ave

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | $\%$ | 14t |  | ${ }^{7}$ | 㙟 |  | 71 | 4 | 7 | 7 | ¢ |  |
| Traffic Volume (veh/h) | 123 | 1688 | 190 | 85 | 2035 | 60 | 119 | 161 | 68 | 136 | 243 | 101 |
| Future Volume (veh/h) | 123 | 1688 | 190 | 85 | 2035 | 60 | 119 | 161 | 68 | 136 | 243 | 101 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1885 | 1826 | 1885 | 1885 | 1841 | 1841 | 1856 | 1870 | 1826 | 1870 | 1870 | 1856 |
| Adj Flow Rate, veh/h | 132 | 1815 | 184 | 91 | 2188 | 59 | 128 | 173 | 50 | 146 | 261 | 98 |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Percent Heavy Veh, \% | 1 | 5 | 1 | 1 | 4 | 4 | 3 | 2 | 5 | 2 | 2 | 3 |
| Cap, veh/h | 149 | 2566 | 259 | 107 | 2688 | 72 | 163 | 352 | 291 | 281 | 273 | 102 |
| Arrive On Green | 0.03 | 0.18 | 0.18 | 0.12 | 1.00 | 1.00 | 0.05 | 0.19 | 0.19 | 0.07 | 0.21 | 0.21 |
| Sat Flow, veh/h | 1795 | 4601 | 464 | 1795 | 5031 | 135 | 3428 | 1870 | 1547 | 1781 | 1296 | 487 |
| Grp Volume(v), veh/h | 132 | 1309 | 690 | 91 | 1455 | 792 | 128 | 173 | 50 | 146 | 0 | 359 |
| Grp Sat Flow(s),veh/h/ln | 1795 | 1662 | 1742 | 1795 | 1675 | 1816 | 1714 | 1870 | 1547 | 1781 | 0 | 1783 |
| Q Serve(g_s), s | 15.4 | 77.6 | 78.1 | 10.4 | 0.0 | 0.0 | 7.8 | 17.4 | 5.7 | 13.9 | 0.0 | 41.8 |
| Cycle Q Clear (g_c), s | 15.4 | 77.6 | 78.1 | 10.4 | 0.0 | 0.0 | 7.8 | 17.4 | 5.7 | 13.9 | 0.0 | 41.8 |
| Prop In Lane | 1.00 |  | 0.27 | 1.00 |  | 0.07 | 1.00 |  | 1.00 | 1.00 |  | 0.27 |
| Lane Grp Cap(c), veh/h | 149 | 1854 | 972 | 107 | 1790 | 970 | 163 | 352 | 291 | 281 | 0 | 375 |
| V/C Ratio(X) | 0.89 | 0.71 | 0.71 | 0.85 | 0.81 | 0.82 | 0.79 | 0.49 | 0.17 | 0.52 | 0.00 | 0.96 |
| Avail Cap(c_a), veh/h | 156 | 1854 | 972 | 173 | 1790 | 970 | 305 | 443 | 366 | 281 | 0 | 388 |
| HCM Platoon Ratio | 0.33 | 0.33 | 0.33 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 0.65 | 0.65 | 0.65 | 0.78 | 0.78 | 0.78 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 101.1 | 69.5 | 69.8 | 91.6 | 0.0 | 0.0 | 99.0 | 76.3 | 71.5 | 63.5 | 0.0 | 81.9 |
| Incr Delay (d2), s/veh | 29.7 | 1.5 | 2.9 | 15.9 | 3.3 | 6.0 | 8.1 | 1.1 | 0.3 | 1.7 | 0.0 | 34.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ( $50 \%$ ),veh/ln | 8.7 | 35.3 | 37.7 | 5.1 | 0.8 | 1.6 | 3.7 | 8.6 | 2.3 | 6.5 | 0.0 | 22.9 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 130.8 | 71.0 | 72.6 | 107.6 | 3.3 | 6.0 | 107.0 | 77.3 | 71.8 | 65.2 | 0.0 | 115.9 |
| LnGrp LOS | F | E | E | F | A | A | F | E | E | E | A | F |
| Approach Vol, veh/h |  | 2131 |  |  | 2338 |  |  | 351 |  |  | 505 |  |
| Approach Delay, s/veh |  | 75.3 |  |  | 8.3 |  |  | 87.4 |  |  | 101.3 |  |
| Approach LOS |  | E |  |  | A |  |  | F |  |  | F |  |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), $s$ | 24.2 | 119.0 | 21.0 | 45.8 | 19.3 | 123.9 | 16.3 | 50.5 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), $s$ | 6.8 | 6.8 | * 6.3 | * 6.3 | 6.8 | 6.8 | * 6.3 | * 6.3 |  |  |  |  |
| Max Green Setting (Gmax), s | 18.2 | 101.2 | * 15 | *50 | 20.2 | 99.2 | *19 | * 46 |  |  |  |  |
| Max Q Clear Time (g_c+11), s | 17.4 | 2.0 | 15.9 | 19.4 | 12.4 | 80.1 | 9.8 | 43.8 |  |  |  |  |
| Green Ext Time ( p c c , s | 0.0 | 34.7 | 0.0 | 1.2 | 0.1 | 12.9 | 0.2 | 0.4 |  |  |  |  |

Intersection Summary
HCM 6th CtrI Delay
49.1

HCM 6th LOS
D

* Notes

HCM 6th Signalized Intersection Summary
2：Rome Ave \＆Hillsborough Ave

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | 1 | 平嘅 |  | 7 | 舟食 |  | 41 | 4 | F | 7 | F |  |
| Traffic Volume（veh／h） | 238 | 2102 | 95 | 59 | 1908 | 143 | 119 | 298 | 78 | 85 | 143 | 72 |
| Future Volume（veh／h） | 238 | 2102 | 95 | 59 | 1908 | 143 | 119 | 298 | 78 | 85 | 143 | 72 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1885 | 1870 | 1885 | 1870 | 1841 | 1841 | 1885 | 1885 | 1885 | 1856 | 1856 | 1870 |
| Adj Flow Rate，veh／h | 256 | 2260 | 91 | 63 | 2052 | 138 | 128 | 320 | 58 | 91 | 154 | 69 |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Percent Heavy Veh，\％ | 1 | 2 | 1 | 2 | 4 | 4 | 1 | 1 | 1 | 3 | 3 | 2 |
| Cap，veh／h | 271 | 3124 | 125 | 78 | 2468 | 165 | 162 | 446 | 378 | 116 | 192 | 86 |
| Arrive On Green | 0.30 | 1.00 | 1.00 | 0.09 | 1.00 | 1.00 | 0.05 | 0.24 | 0.24 | 0.16 | 0.16 | 0.16 |
| Sat Flow，veh／h | 1795 | 5036 | 202 | 1781 | 4811 | 322 | 3483 | 1885 | 1598 | 997 | 1214 | 544 |
| Grp Volume（v），veh／h | 256 | 1524 | 827 | 63 | 1425 | 765 | 128 | 320 | 58 | 91 | 0 | 223 |
| Grp Sat Flow（s），veh／h／ln | 1795 | 1702 | 1834 | 1781 | 1675 | 1783 | 1742 | 1885 | 1598 | 997 | 0 | 1758 |
| Q Serve（g＿s），s | 27.9 | 0.0 | 0.0 | 6.9 | 0.0 | 0.0 | 7.3 | 31.2 | 5.8 | 16.1 | 0.0 | 24.5 |
| Cycle Q Clear（g＿c），s | 27.9 | 0.0 | 0.0 | 6.9 | 0.0 | 0.0 | 7.3 | 31.2 | 5.8 | 31.7 | 0.0 | 24.5 |
| Prop In Lane | 1.00 |  | 0.11 | 1.00 |  | 0.18 | 1.00 |  | 1.00 | 1.00 |  | 0.31 |
| Lane Grp Cap（c），veh／h | 271 | 2112 | 1138 | 78 | 1719 | 915 | 162 | 446 | 378 | 116 | 0 | 279 |
| V／C Ratio（X） | 0.94 | 0.72 | 0.73 | 0.81 | 0.83 | 0.84 | 0.79 | 0.72 | 0.15 | 0.78 | 0.00 | 0.80 |
| Avail Cap（c＿a），veh／h | 316 | 2112 | 1138 | 135 | 1719 | 915 | 186 | 459 | 389 | 116 | 0 | 279 |
| HCM Platoon Ratio | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 0.52 | 0.52 | 0.52 | 0.83 | 0.83 | 0.83 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay（d），s／veh | 69.0 | 0.0 | 0.0 | 90.5 | 0.0 | 0.0 | 94.4 | 70.2 | 60.5 | 92.9 | 0.0 | 81.1 |
| Incr Delay（d2），s／veh | 22.0 | 1.1 | 2.2 | 15.1 | 4.0 | 7.6 | 17.8 | 5.2 | 0.2 | 28.5 | 0.0 | 15.2 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（ $50 \%$ ），veh／ln | 13.0 | 0.3 | 0.7 | 3.4 | 1.0 | 1.9 | 3.7 | 15.9 | 2.4 | 5.7 | 0.0 | 12.4 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 91.0 | 1.1 | 2.2 | 105.6 | 4.0 | 7.6 | 112.2 | 75.4 | 60.7 | 121.4 | 0.0 | 96.3 |
| LnGrp LOS | F | A | A | F | A | A | F | E | E | F | A | F |
| Approach Vol，veh／h |  | 2607 |  |  | 2253 |  |  | 506 |  |  | 314 |  |
| Approach Delay，s／veh |  | 10.3 |  |  | 8.1 |  |  | 83.0 |  |  | 103.6 |  |
| Approach LOS |  | B |  |  | A |  |  | F |  |  | F |  |
| Timer－Assigned Phs | 1 | 2 |  | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Phs Duration（ $G+Y+R \mathrm{c}$ ），$s$ | 37.0 | 109.4 |  | 53.6 | 15.5 | 130.9 | 15.6 | 38.0 |  |  |  |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ）， s | 6.8 | 6.8 |  | ＊ 6.3 | 6.8 | 6.8 | ＊ 6.3 | ＊ 6.3 |  |  |  |  |
| Max Green Setting（Gmax），s | 35.2 | 96.2 |  | ＊ 49 | 15.2 | 116.2 | ＊ 11 | ＊ 32 |  |  |  |  |
| Max Q Clear Time（g＿ctl1），s | 29.9 | 2.0 |  | 33.2 | 8.9 | 2.0 | 9.3 | 33.7 |  |  |  |  |
| Green Ext Time（p＿c），s | 0.3 | 32.4 |  | 1.8 | 0.0 | 40.1 | 0.0 | 0.0 |  |  |  |  |

Intersection Summary
HCM 6th Ctrl Delay 21.0
HCM 6th LOS
C
Notes HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．

HCM 6th Signalized Intersection Summary
2：Rome Ave \＆Hillsborough Ave
11／17／2023

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL． | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％ | 帏家 |  | 7 | 快 ${ }^{\text {P }}$ |  | 7 | 个 | F | \％ | $\hat{1}$ |  |
| Traffic Volume（veh／h） | 123 | 1691 | 198 | 88 | 2035 | 60 | 156 | 169 | 78 | 136 | 245 | 101 |
| Future Volume（veh／h） | 123 | 1691 | 198 | 88 | 2035 | 60 | 156 | 169 | 78 | 136 | 245 | 101 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1885 | 1826 | 1885 | 1885 | 1841 | 1841 | 1856 | 1870 | 1826 | 1870 | 1870 | 1856 |
| Adj Flow Rate，veh／h | 132 | 1818 | 191 | 95 | 2188 | 59 | 168 | 182 | 59 | 146 | 263 | 98 |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Percent Heavy Veh，\％ | 1 | 5 | 1 | 1 | 4 | 4 | 3 | 2 | 5 | 2 | 2 | 3 |
| Cap，veh／h | 149 | 2488 | 260 | 111 | 2625 | 71 | 203 | 375 | 311 | 289 | 275 | 102 |
| Arrive On Green | 0.03 | 0.18 | 0.18 | 0.12 | 1.00 | 1.00 | 0.06 | 0.20 | 0.20 | 0.07 | 0.21 | 0.21 |
| Sat Flow，veh／h | 1795 | 4584 | 479 | 1795 | 5031 | 135 | 3428 | 1870 | 1547 | 1781 | 1299 | 484 |
| Grp Volume（v），veh／h | 132 | 1316 | 693 | 95 | 1455 | 792 | 168 | 182 | 59 | 146 | 0 | 361 |
| Grp Sat Flow（s），veh／h／ln | 1795 | 1662 | 1740 | 1795 | 1675 | 1816 | 1714 | 1870 | 1547 | 1781 | 0 | 1783 |
| Q Serve（g＿s），s | 15.4 | 78.5 | 79.1 | 10.9 | 0.0 | 0.0 | 10.2 | 18.1 | 6.7 | 13.7 | 0.0 | 42.0 |
| Cycle Q Clear（g＿c），s | 15.4 | 78.5 | 79.1 | 10.9 | 0.0 | 0.0 | 10.2 | 18.1 | 6.7 | 13.7 | 0.0 | 42.0 |
| Prop In Lane | 1.00 |  | 0.28 | 1.00 |  | 0.07 | 1.00 |  | 1.00 | 1.00 |  | 0.27 |
| Lane Grp Cap（c），veh／h | 149 | 1804 | 944 | 111 | 1748 | 948 | 203 | 375 | 311 | 289 | 0 | 377 |
| VIC Ratio（X） | 0.89 | 0.73 | 0.73 | 0.86 | 0.83 | 0.84 | 0.83 | 0.48 | 0.19 | 0.50 | 0.00 | 0.96 |
| Avail Cap（c＿a），veh／h | 156 | 1804 | 944 | 173 | 1748 | 948 | 305 | 443 | 366 | 289 | 0 | 388 |
| HCM Platoon Ratio | 0.33 | 0.33 | 0.33 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 0.64 | 0.64 | 0.64 | 0.78 | 0.78 | 0.78 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay（d），s／veh | 101.1 | 71.6 | 71.9 | 91.2 | 0.0 | 0.0 | 97.7 | 74.3 | 69.7 | 61.7 | 0.0 | 81.9 |
| Incr Delay（d2），s／veh | 29.4 | 1.7 | 3.3 | 17.7 | 3.8 | 6.9 | 11.0 | 1.0 | 0.3 | 1.4 | 0.0 | 34.3 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 8.7 | 35.8 | 38.1 | 5.3 | 0.9 | 1.8 | 4.9 | 8.9 | 2.7 | 6.4 | 0.0 | 23.1 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 130.5 | 73.3 | 75.1 | 108.9 | 3.8 | 6.9 | 108.7 | 75.3 | 70.0 | 63.1 | 0.0 | 116.1 |
| LnGrp LOS | F | E | E | F | A | A | F | E | E | E | A | F |
| Approach Vol，veh／h |  | 2141 |  |  | 2342 |  |  | 409 |  |  | 507 |  |
| Approach Delay，s／veh |  | 77.4 |  |  | 9.1 |  |  | 88.2 |  |  | 100.9 |  |
| Approach LOS |  | E |  |  | A |  |  | F |  |  | F |  |
| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Phs Duration（ $G+Y+R \mathrm{c})$ ，$s$ | 24.2 | 116.3 | 21.0 | 48.4 | 19.7 | 120.8 | 18.7 | 50.7 |  |  |  |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ），s | 6.8 | 6.8 | ＊ 6.3 | ＊ 6.3 | 6.8 | 6.8 | ＊ 6.3 | ＊ 6.3 |  |  |  |  |
| Max Green Setting（Gmax），s | 18.2 | 101.2 | ＊15 | ＊ 50 | 20.2 | 99.2 | ＊ 19 | ＊46 |  |  |  |  |
| Max Q Clear Time（g＿ct1），s | 17.4 | 2.0 | 15.7 | 20.1 | 12.9 | 81.1 | 12.2 | 44.0 |  |  |  |  |
| Green Ext Time（p＿c），s | 0.0 | 34.7 | 0.0 | 1.2 | 0.1 | 12.5 | 0.3 | 0.4 |  |  |  |  |

Intersection Summary
HCM 6th Ctrl Delay 50.8
HCM 6th LOS
D

[^1]HCM 6th Signalized Intersection Summary
2: Rome Ave \& Hillsborough Ave

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | 1 | 性 |  | 4 | 14¢ |  | ${ }^{7 \%}$ | 4 | 7 | \% | F |  |
| Traffic Volume (veh/h) | 238 | 2112 | 119 | 68 | 1908 | 143 | 141 | 303 | 84 | 85 | 151 | 72 |
| Future Volume (veh/h) | 238 | 2112 | 119 | 68 | 1908 | 143 | 141 | 303 | 84 | 85 | 151 | 72 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1885 | 1870 | 1885 | 1870 | 1841 | 1841 | 1885 | 1885 | 1885 | 1856 | 1856 | 1870 |
| Adj Flow Rate, veh/h | 256 | 2271 | 115 | 73 | 2052 | 138 | 152 | 326 | 62 | 91 | 162 | 69 |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Percent Heavy Veh, \% | 1 | 2 | 1 | 2 | 4 | 4 | 1 | 1 | 1 | 3 | 3 | 2 |
| Cap, veh/h | 271 | 3026 | 152 | 88 | 2436 | 163 | 185 | 458 | 389 | 120 | 196 | 83 |
| Arrive On Green | 0.30 | 1.00 | 1.00 | 0.10 | 1.00 | 1.00 | 0.05 | 0.24 | 0.24 | 0.16 | 0.16 | 0.16 |
| Sat Flow, veh/h | 1795 | 4979 | 250 | 1781 | 4811 | 322 | 3483 | 1885 | 1598 | 988 | 1235 | 526 |
| Grp Volume(v), veh/h | 256 | 1548 | 838 | 73 | 1425 | 765 | 152 | 326 | 62 | 91 | 0 | 231 |
| Grp Sat Flow(s), veh/h/ln | 1795 | 1702 | 1825 | 1781 | 1675 | 1783 | 1742 | 1885 | 1598 | 988 | 0 | 1761 |
| Q Serve(g_s), s | 27.9 | 0.0 | 0.0 | 8.0 | 0.0 | 0.0 | 8.6 | 31.6 | 6.1 | 17.0 | 0.0 | 25.4 |
| Cycle Q Clear(g_c), s | 27.9 | 0.0 | 0.0 | 8.0 | 0.0 | 0.0 | 8.6 | 31.6 | 6.1 | 31.7 | 0.0 | 25.4 |
| Prop In Lane | 1.00 |  | 0.14 | 1.00 |  | 0.18 | 1.00 |  | 1.00 | 1.00 |  | 0.30 |
| Lane Grp Cap(c), veh/h | 271 | 2069 | 1109 | 88 | 1696 | 903 | 185 | 458 | 389 | 120 | 0 | 279 |
| V/C Ratio(X) | 0.94 | 0.75 | 0.76 | 0.83 | 0.84 | 0.85 | 0.82 | 0.71 | 0.16 | 0.76 | 0.00 | 0.83 |
| Avail Cap(c_a), veh/h | 316 | 2069 | 1109 | 135 | 1696 | 903 | 186 | 459 | 389 | 120 | 0 | 279 |
| HCM Platoon Ratio | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 0.50 | 0.50 | 0.50 | 0.83 | 0.83 | 0.83 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 69.0 | 0.0 | 0.0 | 89.2 | 0.0 | 0.0 | 93.7 | 69.2 | 59.6 | 92.2 | 0.0 | 81.5 |
| Incr Delay (d2), s/veh | 21.4 | 1.3 | 2.5 | 18.1 | 4.4 | 8.2 | 24.2 | 5.1 | 0.2 | 24.0 | 0.0 | 18.3 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/in | 12.9 | 0.4 | 0.8 | 4.0 | 1.0 | 2.1 | 4.6 | 16.1 | 2.5 | 5.6 | 0.0 | 13.1 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay (d), s/veh | 90.4 | 1.3 | 2.5 | 107.4 | 4.4 | 8.2 | 118.0 | 74.3 | 59.8 | 116.2 | 0.0 | 99.8 |
| LnGrp LOS | F | A | A | F | A | A | F | E | E | F | A | F |
| Approach Vol, veh/h |  | 2642 |  |  | 2263 |  |  | 540 |  |  | 322 |  |
| Approach Delay, s/veh |  | 10.3 |  |  | 9.0 |  |  | 84.9 |  |  | 104.4 |  |
| Approach LOS |  | B |  |  | A |  |  | F |  |  | F |  |
| Timer-Assigned Phs | 1 | 2 |  | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), $s$ | 37.0 | 108.1 |  | 54.9 | 16.7 | 128.3 | 16.9 | 38.0 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ) , $s$ | 6.8 | 6.8 |  | * 6.3 | 6.8 | 6.8 | * 6.3 | * 6.3 |  |  |  |  |
| Max Green Setting (Gmax), s | 35.2 | 96.2 |  | * 49 | 15.2 | 116.2 | * 11 | *32 |  |  |  |  |
| Max Q Clear Time (g_c+11), s | 29.9 | 2.0 |  | 33.6 | 10.0 | 2.0 | 10.6 | 33.7 |  |  |  |  |
| Green Ext Time (p_c), s | 0.3 | 32.4 |  | 1.9 | 0.1 | 41.8 | 0.0 | 0.0 |  |  |  |  |

Intersection Summary
HCM 6th Ctrl Delay

## 22.0

HCM 6th LOS
C
Notes

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

HCM 6th Signalized Intersection Summary
3：Lee PI \＆Hillsborough Ave

|  | 4 |  | \％ | 6 | $4$ | 4 | 4 | $\dagger$ | \％ | ＊ | $\frac{1}{\dagger}$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | 平番令 |  | 7 | 坐个食 |  |  | 4 |  |  | 4 |  |
| Traffic Volume（veh／h） | 5 | 1914 | 5 | 74 | 2364 | 4 | 22 | 2 | 5 | 47 | 5 | 0 |
| Future Volume（veh／h） | 5 | 1914 | 5 | 74 | 2364 | 4 | 22 | 2 | 5 | 47 | 5 | 0 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1885 | 1826 | 1885 | 1885 | 1841 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 |
| Adj Flow Rate，veh／h | 5 | 2036 | 5 | 79 | 2515 | 4 | 23 | 2 | 5 | 50 | 5 | 0 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Percent Heavy Veh，\％ | 1 | 5 | 1 | 1 | 4 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap，veh／h | 137 | 4272 | 10 | 250 | 4402 | 7 | 87 | 9 | 13 | 100 | 7 | 0 |
| Arrive On Green | 0.01 | 1.00 | 1.00 | 0.02 | 0.85 | 0.85 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | 0.00 |
| Sat Flow，veh／h | 1795 | 5134 | 13 | 1795 | 5181 | 8 | 1207 | 198 | 281 | 1430 | 143 | 0 |
| Grp Volume（v），veh／h | 5 | 1318 | 723 | 79 | 1626 | 893 | 30 | 0 | 0 | 55 | 0 | 0 |
| Grp Sat Flow（s），veh／h／ln | 1795 | 1662 | 1824 | 1795 | 1675 | 1839 | 1687 | 0 | 0 | 1573 | 0 | 0 |
| Q Serve（g＿s），s | 0.1 | 0.0 | 0.0 | 1.4 | 29.8 | 29.8 | 0.0 | 0.0 | 0.0 | 3.6 | 0.0 | 0.0 |
| Cycle Q Clear $\mathrm{g}_{\text {＿}} \mathrm{c}$ ），s | 0.1 | 0.0 | 0.0 | 1.4 | 29.8 | 29.8 | 3.4 | 0.0 | 0.0 | 7.0 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.01 | 1.00 |  | 0.00 | 0.77 |  | 0.17 | 0.91 |  | 0.00 |
| Lane Grp Cap（c），veh／h | 137 | 2765 | 1517 | 250 | 2846 | 1563 | 110 | 0 | 0 | 107 | 0 | 0 |
| VIC Ratio（X） | 0.04 | 0.48 | 0.48 | 0.32 | 0.57 | 0.57 | 0.27 | 0.00 | 0.00 | 0.51 | 0.00 | 0.00 |
| Avail Cap（c＿a），veh／h | 221 | 2765 | 1517 | 345 | 2846 | 1563 | 240 | 0 | 0 | 235 | 0 | 0 |
| HCM Platoon Ratio | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 0.66 | 0.66 | 0.66 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay（d），s／veh | 4.4 | 0.0 | 0.0 | 2.3 | 4.6 | 4.6 | 96.9 | 0.0 | 0.0 | 98.5 | 0.0 | 0.0 |
| Incr Delay（d2），s／veh | 0.1 | 0.4 | 0.7 | 0.7 | 0.8 | 1.5 | 1.3 | 0.0 | 0.0 | 3.8 | 0.0 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 0.0 | 0.1 | 0.3 | 0.4 | 8.6 | 9.7 | 1.6 | 0.0 | 0.0 | 3.1 | 0.0 | 0.0 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 4.5 | 0.4 | 0.7 | 3.0 | 5.5 | 6.1 | 98.2 | 0.0 | 0.0 | 102.2 | 0.0 | 0.0 |
| LnGrp LOS | A | A | A | A | A | A | F | A | A | F | A | A |
| Approach Vol，veh／h |  | 2046 |  |  | 2598 |  |  | 30 |  |  | 55 |  |
| Approach Delay，s／veh |  | 0.5 |  |  | 5.6 |  |  | 98.2 |  |  | 102.2 |  |
| Approach LOS |  | A |  |  | A |  |  | F |  |  | F |  |
| Timer－Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration（ $G+Y+R \mathrm{c}$ ），$s$ | 8.2 | 185.3 |  | 16.5 | 11.9 | 181.6 |  | 16.5 |  |  |  |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ）， s | 6.9 | 6.9 |  | ＊ 6.6 | 6.9 | 6.9 |  | ＊ 6.6 |  |  |  |  |
| Max Green Setting（Gmax），s | 11.1 | 150.1 |  | ＊ 28 | 16.1 | 145.1 |  | ＊ 28 |  |  |  |  |
| Max Q Clear Time（g＿c＋11），s | 2.1 | 31.8 |  | 5.4 | 3.4 | 2.0 |  | 9.0 |  |  |  |  |
| Green Ext Time（p＿c），s | 0.0 | 48.5 |  | 0.1 | 0.1 | 28.2 |  | 0.2 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctri Delay |  |  | 5.1 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | A |  |  |  |  |  |  |  |  |  |

Notes
＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．

HCM 6th Signalized Intersection Summary
3：Lee PI \＆Hillsborough Ave
11／17／2023

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | 1 | 个中t |  | \％ | 个中b |  |  | ¢ |  |  | ${ }_{4}$ |  |
| Traffic Volume（veh／h） | 18 | 2184 | 10 | 81 | 2158 | 14 | 37 | 1 | 11 | 13 | 0 | 3 |
| Future Volume（veh／h） | 18 | 2184 | 10 | 81 | 2158 | 14 | 37 | 1 | 11 | 13 | 0 | 3 |
| Initial $\mathrm{Q}(\mathrm{Qb})$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／h | 1811 | 1870 | 1885 | 1885 | 1841 | 1885 | 1856 | 1885 | 1885 | 1885 | 1885 | 1885 |
| Adj Flow Rate，veh／h | 19 | 2275 | 10 | 84 | 2248 | 15 | 39 | 1 | 11 | 14 | 0 | 3 |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Percent Heavy Veh，\％ | 6 | 2 | 1 | 1 | 4 | 1 | 3 | 1 | 1 | 1 | 1 | 1 |
| Cap，veh／h | 177 | 4326 | 19 | 216 | 4289 | 29 | 86 | 4 | 16 | 93 | 3 | 14 |
| Arrive On Green | 0.03 | 1.00 | 1.00 | 0.02 | 0.83 | 0.83 | 0.05 | 0.05 | 0.05 | 0.05 | 0.00 | 0.05 |
| Sat Flow，veh／h | 1725 | 5247 | 23 | 1795 | 5150 | 34 | 1116 | 89 | 331 | 1231 | 66 | 278 |
| Grp Volume（v），veh／h | 19 | 1476 | 809 | 84 | 1462 | 801 | 51 | 0 | 0 | 17 | 0 | 0 |
| Grp Sat Flow（s）ven／h／ln | 1725 | 1702 | 1866 | 1795 | 1675 | 1835 | 1536 | 0 | 0 | 1575 | 0 | 0 |
| Q Serve（g＿s），s | 0.4 | 0.0 | 0.0 | 1.5 | 25.9 | 25.9 | 4.4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Cycle Q Clear（g＿c），s | 0.4 | 0.0 | 0.0 | 1.5 | 25.9 | 25.9 | 6.4 | 0.0 | 0.0 | 2.0 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.01 | 1.00 |  | 0.02 | 0.76 |  | 0.22 | 0.82 |  | 0.18 |
| Lane Grp Cap（c），veh／h | 177 | 2806 | 1538 | 216 | 2790 | 1528 | 107 | 0 | 0 | 110 | 0 | 0 |
| VIC Ratio（ X ） | 0.11 | 0.53 | 0.53 | 0.39 | 0.52 | 0.52 | 0.48 | 0.00 | 0.00 | 0.15 | 0.00 | 0.00 |
| Avail Cap（c＿a），veh／h | 219 | 2806 | 1538 | 360 | 2790 | 1528 | 243 | 0 | 0 | 244 | 0 | 0 |
| HCM Platoon Ratio | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 0.60 | 0.60 | 0.60 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay（d），s／veh | 4.2 | 0.0 | 0.0 | 2.4 | 5.0 | 5.0 | 93.4 | 0.0 | 0.0 | 91.4 | 0.0 | 0.0 |
| Incr Delay（d2），slveh | 0.2 | 0.4 | 0.8 | 1.1 | 0.7 | 1.3 | 3.3 | 0.0 | 0.0 | 0.6 | 0.0 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ $(50 \%$ ），veh／ln | 0.1 | 0.2 | 0.3 | 0.5 | 7.7 | 8.7 | 2.7 | 0.0 | 0.0 | 0.9 | 0.0 | 0.0 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），siveh | 4.3 | 0.4 | 0.8 | 3.5 | 5.7 | 6.3 | 96.6 | 0.0 | 0.0 | 92.0 | 0.0 | 0.0 |
| LnGrp LOS | A | A | A | A | A | A | F | A | A | F | A | A |
| Approach Vol，veh／h |  | 2304 |  |  | 2347 |  |  | 51 |  |  | 17 |  |
| Approach Delay，s／veh |  | 0.6 |  |  | 5.8 |  |  | 96.6 |  |  | 92.0 |  |
| Approach LOS |  | A |  |  | A |  |  | F |  |  | F |  |


| Timer－Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 10.2 | 173.5 | 16.4 | 11.9 | 171.8 | 16.4 |
| Change Period（Y＋Rc），s | 6.9 | 6.9 | ${ }^{*} 6.6$ | 6.9 | 6.9 | ${ }^{*} 6.6$ |
| Max Green Setting（Gmax），s | 8.1 | 143.1 | ${ }^{*} 28$ | 21.1 | 130.1 | ${ }^{*} 28$ |
| Max Q Clear Time（g＿c＋11），s | 2.4 | 27.9 | 8.4 | 3.5 | 2.0 | 4.0 |
| Green Ext Time（p＿c），s | 0.0 | 36.2 | 0.2 | 0.2 | 37.7 | 0.0 |

Intersection Summary
HCM 6th Ctrl Delay 4.5

HCM 6th LOS A
Notes
＊ HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．

## HCM 6th Signalized Intersection Summary

3：Lee PI \＆Hillsborough Ave
11／17／2023

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | 4 | 平个盛 |  | 7 | 番食 |  | \％ | F |  |  | \＄ |  |
| Traffic Volume（veh／h） | 5 | 1914 | 5 | 74 | 2364 | 4 | 22 | 2 | 5 | 47 | 5 | 0 |
| Future Volume（veh／h） | 5 | 1914 | 5 | 74 | 2364 | 4 | 22 | 2 | 5 | 47 | 5 | 0 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1885 | 1826 | 1885 | 1885 | 1841 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 |
| Adj Flow Rate，veh／h | 5 | 2036 | 5 | 79 | 2515 | 4 | 23 | 2 | 5 | 50 | 5 | 0 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Percent Heavy Veh，\％ | 1 | 5 | 1 | 1 | 4 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap，veh／h | 136 | 4250 | 10 | 249 | 4379 | 7 | 120 | 25 | 62 | 96 | 6 | 0 |
| Arrive On Green | 0.01 | 1.00 | 1.00 | 0.02 | 0.85 | 0.85 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | 0.00 |
| Sat Flow，veh／h | 1795 | 5134 | 13 | 1795 | 5181 | 8 | 1422 | 477 | 1193 | 1218 | 123 | 0 |
| Grp Volume（v），veh／h | 5 | 1318 | 723 | 79 | 1626 | 893 | 23 | 0 | 7 | 55 | 0 | 0 |
| Grp Sat Flow（s），veh／h／ln | 1795 | 1662 | 1824 | 1795 | 1675 | 1839 | 1422 | 0 | 1670 | 1341 | 0 | 0 |
| Q Serve（g＿s），s | 0.1 | 0.0 | 0.0 | 1.4 | 30.6 | 30.7 | 0.0 | 0.0 | 0.8 | 7.9 | 0.0 | 0.0 |
| Cycle Q Clear（g＿c），s | 0.1 | 0.0 | 0.0 | 1.4 | 30.6 | 30.7 | 2.7 | 0.0 | 0.8 | 8.7 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.01 | 1.00 |  | 0.00 | 1.00 |  | 0.71 | 0.91 |  | 0.00 |
| Lane Grp Cap（c），veh／h | 136 | 2751 | 1509 | 249 | 2832 | 1555 | 120 | 0 | 86 | 102 | 0 | 0 |
| V／C Ratio（X） | 0.04 | 0.48 | 0.48 | 0.32 | 0.57 | 0.57 | 0.19 | 0.00 | 0.08 | 0.54 | 0.00 | 0.00 |
| Avail Cap（c＿a），veh／h | 194 | 2751 | 1509 | 319 | 2832 | 1555 | 273 | 0 | 266 | 258 | 0 | 0 |
| HCM Platoon Ratio | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（I） | 0.56 | 0.56 | 0.56 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay（d），s／veh | 4.7 | 0.0 | 0.0 | 2.4 | 4.9 | 4.9 | 95.7 | 0.0 | 94.8 | 99.0 | 0.0 | 0.0 |
| Incr Delay（d2），s／veh | 0.1 | 0.3 | 0.6 | 0.7 | 0.9 | 1.6 | 0.8 | 0.0 | 0.4 | 4.4 | 0.0 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 0.0 | 0.1 | 0.3 | 0.5 | 9.0 | 10.1 | 1.2 | 0.0 | 0.4 | 3.1 | 0.0 | 0.0 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 4.7 | 0.3 | 0.6 | 3.2 | 5.7 | 6.4 | 96.5 | 0.0 | 95.2 | 103.4 | 0.0 | 0.0 |
| LnGrp LOS | A | A | A | A | A | A | F | A | F | F | A | A |
| Approach Vol，veh／h |  | 2046 |  |  | 2598 |  |  | 30 |  |  | 55 |  |
| Approach Delay，s／veh |  | 0.4 |  |  | 5.9 |  |  | 96.2 |  |  | 103.4 |  |
| Approach LOS |  | A |  |  | A |  |  | F |  |  | F |  |
| Timer－Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration（ $G+Y+R \mathrm{c}$ ），$s$ | 8.2 | 184.4 |  | 17.4 | 11.9 | 180.7 |  | 17.4 |  |  |  |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ），$s$ | 6.9 | 6.9 |  | ＊ 6.6 | 6.9 | 6.9 |  | ＊ 6.6 |  |  |  |  |
| Max Green Setting（Gmax），s | 8.1 | 148.1 |  | ＊ 33 | 13.1 | 143.1 |  | ＊ 33 |  |  |  |  |
| Max Q Clear Time（g＿c＋11），s | 2.1 | 32.7 |  | 4.7 | 3.4 | 2.0 |  | 10.7 |  |  |  |  |
| Green Ext Time（p＿c），s | 0.0 | 48.1 |  | 0.1 | 0.1 | 28.2 |  | 0.2 |  |  |  |  |

Intersection Summary

## HCM 6th Ctri Delay 5.2 <br> HCM 6th LOS A

## Notes

＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．

HCM 6th Signalized Intersection Summary
3：Lee PI \＆Hillsborough Ave

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | 7 | 平車家 |  | 7 | 平﨡 |  | 7 | F |  |  | ＊ |  |
| Traffic Volume（veh／h） | 18 | 2184 | 10 | 81 | 2158 | 14 | 37 | 1 | 11 | 13 | 0 | 3 |
| Future Volume（veh／h） | 18 | 2184 | 10 | 81 | 2158 | 14 | 37 | 1 | 11 | 13 | 0 | 3 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1811 | 1870 | 1885 | 1885 | 1841 | 1885 | 1856 | 1885 | 1885 | 1885 | 1885 | 1885 |
| Adj Flow Rate，veh／h | 19 | 2275 | 10 | 84 | 2248 | 15 | 39 | 1 | 11 | 14 | 0 | 3 |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Percent Heavy Veh，\％ | 6 | 2 | 1 | 1 | 4 | 1 | 3 | 1 | 1 | 1 | 1 | 1 |
| Cap，veh／h | 177 | 4326 | 19 | 216 | 4289 | 29 | 110 | 7 | 72 | 82 | 3 | 11 |
| Arrive On Green | 0.03 | 1.00 | 1.00 | 0.02 | 0.83 | 0.83 | 0.05 | 0.05 | 0.05 | 0.05 | 0.00 | 0.05 |
| Sat Flow，veh／h | 1725 | 5247 | 23 | 1795 | 5150 | 34 | 1403 | 135 | 1483 | 1015 | 66 | 232 |
| Grp Volume（v），veh／h | 19 | 1476 | 809 | 84 | 1462 | 801 | 39 | 0 | 12 | 17 | 0 | 0 |
| Grp Sat Flow（s），veh／h／ln | 1725 | 1702 | 1866 | 1795 | 1675 | 1835 | 1403 | 0 | 1618 | 1313 | 0 | 0 |
| Q Serve（g＿s），s | 0.4 | 0.0 | 0.0 | 1.5 | 25.9 | 25.9 | 1.4 | 0.0 | 1.4 | 1.7 | 0.0 | 0.0 |
| Cycle Q Clear（g＿c），s | 0.4 | 0.0 | 0.0 | 1.5 | 25.9 | 25.9 | 4.6 | 0.0 | 1.4 | 3.2 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.01 | 1.00 |  | 0.02 | 1.00 |  | 0.92 | 0.82 |  | 0.18 |
| Lane Grp Cap（c），veh／h | 177 | 2806 | 1538 | 216 | 2790 | 1528 | 110 | 0 | 79 | 97 | 0 | 0 |
| V／C Ratio（X） | 0.11 | 0.53 | 0.53 | 0.39 | 0.52 | 0.52 | 0.35 | 0.00 | 0.15 | 0.18 | 0.00 | 0.00 |
| Avail Cap（c＿a），veh／h | 219 | 2806 | 1538 | 360 | 2790 | 1528 | 255 | 0 | 246 | 246 | 0 | 0 |
| HCM Platoon Ratio | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 0.58 | 0.58 | 0.58 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay（d），s／veh | 4.2 | 0.0 | 0.0 | 2.4 | 5.0 | 5.0 | 92.5 | 0.0 | 91.1 | 92.2 | 0.0 | 0.0 |
| Incr Delay（d2），s／veh | 0.2 | 0.4 | 0.8 | 1.1 | 0.7 | 1.3 | 1.9 | 0.0 | 0.9 | 0.9 | 0.0 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 0.1 | 0.2 | 0.3 | 0.5 | 7.7 | 8.7 | 2.1 | 0.0 | 0.6 | 0.9 | 0.0 | 0.0 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 4.3 | 0.4 | 0.8 | 3.5 | 5.7 | 6.3 | 94.5 | 0.0 | 92.0 | 93.0 | 0.0 | 0.0 |
| LnGrp LOS | A | A | A | A | A | A | F | A | F | F | A | A |
| Approach Vol，veh／h |  | 2304 |  |  | 2347 |  |  | 51 |  |  | 17 |  |
| Approach Delay，s／veh |  | 0.6 |  |  | 5.8 |  |  | 93.9 |  |  | 93.0 |  |
| Approach LOS |  | A |  |  | A |  |  | F |  |  | F |  |
| Timer－Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration（ $G+Y+R \mathrm{c}$ ），$s$ | 10.2 | 173.5 |  | 16.4 | 11.9 | 171.8 |  | 16.4 |  |  |  |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ），s | 6.9 | 6.9 |  | ＊ 6.6 | 6.9 | 6.9 |  | ＊ 6.6 |  |  |  |  |
| Max Green Setting（Gmax），s | 8.1 | 141.1 |  | ＊ 30 | 21.1 | 128.1 |  | ＊ 30 |  |  |  |  |
| Max Q Clear Time（g＿c＋11），s | 2.4 | 27.9 |  | 6.6 | 3.5 | 2.0 |  | 5.2 |  |  |  |  |
| Green Ext Time（ $\mathrm{p}_{2} \mathrm{c}$ ）， s | 0.0 | 36.1 |  | 0.1 | 0.2 | 37.6 |  | 0.0 |  |  |  |  |

Intersection Summary

| HCM 6th Ctrl Delay | 4.5 |
| :--- | ---: |
| HCM 6th LOS | A |

## Notes

＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％ | 平个家 |  | 7 |  |  | \％ | F |  |  | 4 |  |
| Traffic Volume（veh／h） | 5 | 1938 | 5 | 74 | 2372 | 4 | 22 | 2 | 5 | 47 | 5 | 0 |
| Future Volume（veh／h） | 5 | 1938 | 5 | 74 | 2372 | 4 | 22 | 2 | 5 | 47 | 5 | 0 |
| Initial $\mathrm{Q}(\mathrm{Qb})$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1885 | 1826 | 1885 | 1885 | 1841 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 |
| Adj Flow Rate，veh／h | 5 | 2062 | 5 | 79 | 2523 | 4 | 23 | 2 | 5 | 50 | 5 | 0 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Percent Heavy Veh，\％ | 1 | 5 | 1 | 1 | 4 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap，veh／h | 135 | 4250 | 10 | 245 | 4379 | 7 | 120 | 25 | 62 | 96 | 6 | 0 |
| Arrive On Green | 0.01 | 1.00 | 1.00 | 0.02 | 0.85 | 0.85 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | 0.00 |
| Sat Flow，veh／h | 1795 | 5134 | 12 | 1795 | 5181 | 8 | 1422 | 477 | 1193 | 1218 | 123 | 0 |
| Grp Volume（v），veh／h | 5 | 1335 | 732 | 79 | 1631 | 896 | 23 | 0 | 7 | 55 | 0 | 0 |
| Grp Sat Flow（s），veh／h／ln | 1795 | 1662 | 1824 | 1795 | 1675 | 1839 | 1422 | 0 | 1670 | 1341 | 0 | 0 |
| Q Serve（g＿s），s | 0.1 | 0.0 | 0.0 | 1.4 | 30.8 | 30.9 | 0.0 | 0.0 | 0.8 | 7.9 | 0.0 | 0.0 |
| Cycle Q Clear（g＿c），s | 0.1 | 0.0 | 0.0 | 1.4 | 30.8 | 30.9 | 2.7 | 0.0 | 0.8 | 8.7 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.01 | 1.00 |  | 0.00 | 1.00 |  | 0.71 | 0.91 |  | 0.00 |
| Lane Grp Cap（c），veh／h | 135 | 2751 | 1509 | 245 | 2832 | 1555 | 120 | 0 | 86 | 102 | 0 | 0 |
| VIC Ratio（X） | 0.04 | 0.49 | 0.49 | 0.32 | 0.58 | 0.58 | 0.19 | 0.00 | 0.08 | 0.54 | 0.00 | 0.00 |
| Avail Cap（c＿a），veh／h | 193 | 2751 | 1509 | 314 | 2832 | 1555 | 273 | 0 | 266 | 258 | 0 | 0 |
| HCM Platoon Ratio | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 0.54 | 0.54 | 0.54 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay（d），s／veh | 4.7 | 0.0 | 0.0 | 2.4 | 4.9 | 4.9 | 95.7 | 0.0 | 94.8 | 99.0 | 0.0 | 0.0 |
| Incr Delay（d2），s／veh | 0.1 | 0.3 | 0.6 | 0.8 | 0.9 | 1.6 | 0.8 | 0.0 | 0.4 | 4.4 | 0.0 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 0.0 | 0.1 | 0.3 | 0.5 | 9.0 | 10.2 | 1.2 | 0.0 | 0.4 | 3.1 | 0.0 | 0.0 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 4.8 | 0.3 | 0.6 | 3.2 | 5.8 | 6.5 | 96.5 | 0.0 | 95.2 | 103.4 | 0.0 | 0.0 |
| LnGrp LOS | A | A | A | A | A | A | F | A | F | F | A | A |
| Approach Vol，veh／h |  | 2072 |  |  | 2606 |  |  | 30 |  |  | 55 |  |
| Approach Delay，s／veh |  | 0.4 |  |  | 5.9 |  |  | 96.2 |  |  | 103.4 |  |
| Approach LOS |  | A |  |  | A |  |  | F |  |  | F |  |
| Timer－Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration（ $G+Y+R \mathrm{c}$ ），$s$ | 8.2 | 184.4 |  | 17.4 | 11.9 | 180.7 |  | 17.4 |  |  |  |  |
| Change Period（ $Y+R \mathrm{c}$ ），s | 6.9 | 6.9 |  | ＊ 6.6 | 6.9 | 6.9 |  | ＊ 6.6 |  |  |  |  |
| Max Green Setting（Gmax），s | 8.1 | 148.1 |  | ＊ 33 | 13.1 | 143.1 |  | ＊ 33 |  |  |  |  |
| Max Q Clear Time（g＿c＋l1），s | 2.1 | 32.9 |  | 4.7 | 3.4 | 2.0 |  | 10.7 |  |  |  |  |
| Green Ext Time（p＿c），s | 0.0 | 48.5 |  | 0.1 | 0.1 | 29.1 |  | 0.2 |  |  |  |  |

## Intersection Summary

| HCM 6th Ctri Delay | 5.2 |
| :--- | ---: |
| HCM 6th LOS | A |

[^2]HCM 6th Signalized Intersection Summary
3：Lee PI \＆Hillsborough Ave
11／17／2023

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | 7 | 平車阤 |  | 7 | 舟食 |  | 7 | F |  |  | ＊ |  |
| Trafic Volume（veh／h） | 18 | 2198 | 10 | 81 | 2181 | 14 | 37 | 1 | 11 | 13 | 0 | 3 |
| Future Volume（veh／h） | 18 | 2198 | 10 | 81 | 2181 | 14 | 37 | 1 | 11 | 13 | 0 | 3 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1811 | 1870 | 1885 | 1885 | 1841 | 1885 | 1856 | 1885 | 1885 | 1885 | 1885 | 1885 |
| Adj Flow Rate，veh／h | 19 | 2290 | 10 | 84 | 2272 | 15 | 39 | 1 | 11 | 14 | 0 | 3 |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Percent Heavy Veh，\％ | 6 | 2 | 1 | 1 | 4 | 1 | 3 | 1 | 1 | 1 | 1 | 1 |
| Cap，veh／h | 174 | 4326 | 19 | 214 | 4290 | 28 | 110 | 7 | 72 | 82 | 3 | 11 |
| Arrive On Green | 0.03 | 1.00 | 1.00 | 0.02 | 0.83 | 0.83 | 0.05 | 0.05 | 0.05 | 0.05 | 0.00 | 0.05 |
| Sat Flow，veh／h | 1725 | 5247 | 23 | 1795 | 5151 | 34 | 1403 | 135 | 1483 | 1015 | 66 | 232 |
| Grp Volume（v），veh／h | 19 | 1485 | 815 | 84 | 1477 | 810 | 39 | 0 | 12 | 17 | 0 | 0 |
| Grp Sat Flow（s），veh／h／ln | 1725 | 1702 | 1866 | 1795 | 1675 | 1835 | 1403 | 0 | 1618 | 1313 | 0 | 0 |
| Q Serve（g＿s），s | 0.4 | 0.0 | 0.0 | 1.5 | 26.4 | 26.4 | 1.4 | 0.0 | 1.4 | 1.7 | 0.0 | 0.0 |
| Cycle Q Clear（g＿c），s | 0.4 | 0.0 | 0.0 | 1.5 | 26.4 | 26.4 | 4.6 | 0.0 | 1.4 | 3.2 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.01 | 1.00 |  | 0.02 | 1.00 |  | 0.92 | 0.82 |  | 0.18 |
| Lane Grp Cap（c），veh／h | 174 | 2806 | 1538 | 214 | 2790 | 1528 | 110 | 0 | 79 | 97 | 0 | 0 |
| V／C Ratio（X） | 0.11 | 0.53 | 0.53 | 0.39 | 0.53 | 0.53 | 0.35 | 0.00 | 0.15 | 0.18 | 0.00 | 0.00 |
| Avail Cap（c＿a），veh／h | 216 | 2806 | 1538 | 358 | 2790 | 1528 | 255 | 0 | 246 | 246 | 0 | 0 |
| HCM Platoon Ratio | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 0.55 | 0.55 | 0.55 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay（d），s／veh | 4.2 | 0.0 | 0.0 | 2.4 | 5.0 | 5.0 | 92.5 | 0.0 | 91.1 | 92.2 | 0.0 | 0.0 |
| Incr Delay（d2），s／veh | 0.2 | 0.4 | 0.7 | 1.2 | 0.7 | 1.3 | 1.9 | 0.0 | 0.9 | 0.9 | 0.0 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 0.1 | 0.2 | 0.3 | 0.5 | 7.9 | 8.9 | 2.1 | 0.0 | 0.6 | 0.9 | 0.0 | 0.0 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 4.4 | 0.4 | 0.7 | 3.6 | 5.7 | 6.3 | 94.5 | 0.0 | 92.0 | 93.0 | 0.0 | 0.0 |
| LnGrp LOS | A | A | A | A | A | A | F | A | F | F | A | A |
| Approach Vol，veh／h |  | 2319 |  |  | 2371 |  |  | 51 |  |  | 17 |  |
| Approach Delay，s／veh |  | 0.5 |  |  | 5.9 |  |  | 93.9 |  |  | 93.0 |  |
| Approach LOS |  | A |  |  | A |  |  | F |  |  | F |  |
| Timer－Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration（ $G+Y+R \mathrm{c}$ ），$s$ | 10.2 | 173.5 |  | 16.4 | 11.9 | 171.8 |  | 16.4 |  |  |  |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ）， s | 6.9 | 6.9 |  | ＊ 6.6 | 6.9 | 6.9 |  | ＊ 6.6 |  |  |  |  |
| Max Green Setting（Gmax），s | 8.1 | 141.1 |  | ＊ 30 | 21.1 | 128.1 |  | ＊ 30 |  |  |  |  |
| Max Q Clear Time（g＿c＋11），s | 2.4 | 28.4 |  | 6.6 | 3.5 | 2.0 |  | 5.2 |  |  |  |  |
| Green Ext Time（p＿c），$s$ | 0.0 | 37.1 |  | 0.1 | 0.2 | 38.3 |  | 0.0 |  |  |  |  |

Intersection Summary
HCM 6th Ctrl Delay
4.5

HCM 6th LOS
A
Notes
＊HCM 6 th computational engine requires equal clearance times for the phases crossing the barrier．

PERCENT CONSUMED CALCULATIONS

TABLE A-1
PROPORTIONATE SHARE CALCULATION

| Intersection | Time Period | Critical <br> Movement | LOS E Lane Group Capacity | LOS D <br> Lane Group <br> Capacity (1) | New Project Trips |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Hillsborough Ave and Armenia Ave | AM | WB Left | 235 | 208 | 4 |
|  |  | WB Thru | 2,581 | 2,284 | 29 |
|  |  | NB Left | 202 | 179 | 0 |
|  |  | SB Through/Right | 717 | $\underline{635}$ | $\underline{0}$ |
|  |  |  |  | 3,306 | 33 |
|  |  |  |  | \% Consumed | 1.00\% |
|  | PM | EB Left | 466 | 412 | 0 |
|  |  | EB Through | 2,639 | 2,336 | 26 |
|  |  | WB Through | 2,232 | 1,975 | 18 |
|  |  | NB Left | 239 | 212 | 0 |
|  |  | NB Through/Right | 750 | 664 | 4 |
|  |  |  |  | 5,599 | 48 |
|  |  |  |  | \% Consumed | 0.86\% |
| Hillsborough Ave and Rome Ave | AM | EB Left | 152 | 135 | 0 |
|  |  | WB Thru/Right | 2,468 | 2,184 | 0 |
|  |  | NB Left | 250 | 221 | 37 |
|  |  | SB Through/Right | 389 | 344 | $\underline{2}$ |
|  |  |  |  | 2,884 | 39 |
|  |  |  |  | \% Consumed | 1.35\% |
|  | PM | EB Left | 286 | 253 | 0 |
|  |  | WB Through/Right | 2,509 | 2,220 | 0 |
|  |  | NB Through | 435 | 385 | 5 |
|  |  | SB Left | 96 | 85 | $\underline{0}$ |
|  |  |  |  | 2,943 | 5 |
|  |  |  |  | \% Consumed | 0.17\% |
| Hillsborough Ave and Lee Place | AM | WB Left | 174 | 154 | 0 |
|  |  | WB Thru/Right | 4,139 | 3,663 | 8 |
|  |  | SB Left/Through/ | 93 | 82 | $\underline{0}$ |
|  |  | Right |  | 3,899 | 8 |
|  |  |  |  | \% Consumed | 0.21\% |
|  | PM | EB Thru/Right | 4,078 | 3,609 | 14 |
|  |  | WB Left | 166 | 147 | 0 |
|  |  | WB Thru/Right | 4,136 | 3,660 | 23 |
|  |  | NB Left | 68 | 60 | $\underline{0}$ |
|  |  |  |  | 7,476 | 37 |
|  |  |  |  | \% Consumed | 0.49\% |

(1) Adjusted by 0.885

HCM Signalized Intersection Capacity Analysis
1: Armenia Ave \& Hillsborough Ave

|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |

HCM Signalized Intersection Capacity Analysis
1: Armenia Ave \& Hillsborough Ave

|  | $\dagger$ | $\rightarrow$ |  | 7 |  |  | 4 | $\dagger$ | 7 | - | $\downarrow$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% 71 |  | $\overline{7}$ | \% ${ }^{14}$ | 444 | $\overline{7}$ | ${ }^{1}$ | 个t |  | 7 | 个t |  |
| Traffic Volume (vph) | 432 | 2054 | 176 | 124 | 1850 | 144 | 215 | 606 | 112 | 135 | 345 | 150 |
| Future Volume (vph) | 432 | 2054 | 176 | 124 | 1850 | 144 | 215 | 606 | 112 | 135 | 345 | 150 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 6.9 | 6.9 | 6.9 | 6.9 | 6.9 | 6.9 | 6.4 | 6.4 |  | 6.4 | 6.4 |  |
| Lane Util. Factor | 0.97 | 0.91 | 1.00 | 0.97 | 0.91 | 1.00 | 1.00 | 0.95 |  | 1.00 | 0.95 |  |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.98 |  | 1.00 | 0.95 |  |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 |  |
| Satd. Flow (prot) | 3467 | 5085 | 1599 | 3400 | 4988 | 1553 | 1787 | 3457 |  | 1752 | 3412 |  |
| Fit Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.18 | 1.00 |  | 0.10 | 1.00 |  |
| Satd. Flow (perm) | 3467 | 5085 | 1599 | 3400 | 4988 | 1553 | 340 | 3457 |  | 192 | 3412 |  |
| Peak-hour factor, PHF | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Adj. Flow (vph) | 441 | 2096 | 180 | 127 | 1888 | 147 | 219 | 618 | 114 | 138 | 352 | 153 |
| RTOR Reduction (vph) | , | 0 | 44 | 0 | 0 | 71 | 0 | 8 | 0 | 0 | 24 | 0 |
| Lane Group Flow (vph) | 441 | 2096 | 136 | 127 | 1888 | 76 | 219 | 724 | 0 | 138 | 481 | ( |
| Heavy Vehicles (\%) | 1\% | 2\% | 1\% | 3\% | 4\% | 4\% | 1\% | 2\% | 2\% | 3\% | 1\% | 1\% |
| Turn Type | Prot | NA | Perm | Prot | NA | Perm | pm+pt | NA |  | pm+pt | NA |  |
| Protected Phases | 1 | 6 |  | 5 | 2 |  | 7 | , |  | 3 | 8 |  |
| Permitted Phases |  |  | 6 |  |  | 2 | 4 |  |  | 8 |  |  |
| Actuated Green, G (s) | 26.9 | 103.8 | 103.8 | 12.6 | 89.5 | 89.5 | 62.0 | 43.4 |  | 52.0 | 38.4 |  |
| Effective Green, g (s) | 26.9 | 103.8 | 103.8 | 12.6 | 89.5 | 89.5 | 62.0 | 43.4 |  | 52.0 | 38.4 |  |
| Actuated g/C Ratio | 0.13 | 0.52 | 0.52 | 0.06 | 0.45 | 0.45 | 0.31 | 0.22 |  | 0.26 | 0.19 |  |
| Clearance Time (s) | 6.9 | 6.9 | 6.9 | 6.9 | 6.9 | 6.9 | 6.4 | 6.4 |  | 6.4 | 6.4 |  |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Lane Grp Cap (vph) | 466 | 2639 | 829 | 214 | 2232 | 694 | 239 | 750 |  | 156 | 655 |  |
| v/s Ratio Prot | c0.13 | c0.41 |  | 0.04 | c0.38 |  | c0.08 | c0.21 |  | 0.06 | 0.14 |  |
| v/s Ratio Perm |  |  | 0.09 |  |  | 0.05 | 0.20 |  |  | 0.17 |  |  |
| v/c Ratio | 0.95 | 0.79 | 0.16 | 0.59 | 0.85 | 0.11 | 0.92 | 0.97 |  | 0.88 | 0.73 |  |
| Uniform Delay, d1 | 85.8 | 39.4 | 25.3 | 91.2 | 49.1 | 32.1 | 57.5 | 77.6 |  | 62.3 | 76.0 |  |
| Progression Factor | 1.00 | 1.00 | 1.00 | 0.69 | 1.51 | 4.42 | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Incremental Delay, d2 | 28.3 | 2.6 | 0.4 | 2.0 | 2.0 | 0.1 | 36.1 | 24.4 |  | 40.3 | 4.3 |  |
| Delay (s) | 114.2 | 41.9 | 25.7 | 64.8 | 76.2 | 142.1 | 93.5 | 102.0 |  | 102.5 | 80.3 |  |
| Level of Service | F | D | C | E | E | F | F | F |  | F | F |  |
| Approach Delay (s) |  | 52.6 |  |  | 80.0 |  |  | 100.1 |  |  | 85.0 |  |
| Approach LOS |  | D |  |  | E |  |  | F |  |  | F |  |

Intersection Summary

| HCM 2000 Control Delay | 71.9 | HCM 2000 Level of Service | E |
| :--- | ---: | :--- | ---: |
| HCM 200 Volume to Capacity ratio | 0.92 |  | 26.6 |
| Actuated Cycle Length (s) | 200.0 | Sum of lost time (s) | F |
| Intersection Capacity Utilization | $98.0 \%$ | ICU Level of Service |  |
| Analysis Period (min) | 15 |  |  |
| c Critical Lane Group |  |  |  |



HCM Signalized Intersection Capacity Analysis
2：Rome Ave \＆Hillsborough Ave

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | 7 | 雨台 |  | 7 | 飡官 |  | 97 | 4 | F | \％ | f |  |
| Traffic Volume（vph） | 238 | 2112 | 119 | 68 | 1908 | 143 | 141 | 303 | 84 | 85 | 151 | 72 |
| Future Volume（vph） | 238 | 2112 | 119 | 68 | 1908 | 143 | 141 | 303 | 84 | 85 | 151 | 72 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time（s） | 6.8 | 6.8 |  | 6.8 | 6.8 |  | 6.3 | 6.3 | 6.3 | 6.3 | 6.3 |  |
| Lane Utill．Factor | 1.00 | 0.91 |  | 1.00 | 0.91 |  | 0.97 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Fit | 1.00 | 0.99 |  | 1.00 | 0.99 |  | 1.00 | 1.00 | 0.85 | 1.00 | 0.95 |  |
| Flt Protected | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  |
| Satd．Flow（prot） | 1787 | 5047 |  | 1770 | 4935 |  | 3467 | 1881 | 1599 | 1752 | 1761 |  |
| Fit Permitted | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.36 | 1.00 |  |
| Satd．Flow（perm） | 1787 | 5047 |  | 1770 | 4935 |  | 3467 | 1881 | 1599 | 660 | 1761 |  |
| Peak－hour factor，PHF | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Adj．Flow（vph） | 256 | 2271 | 128 | 73 | 2052 | 154 | 152 | 326 | 90 | 91 | 162 | 77 |
| RTOR Reduction（vph） | 0 | 3 | 0 | 0 | 4 | 0 | 0 | 0 | 69 | 0 | 9 | 0 |
| Lane Group Flow（vph） | 256 | 2396 | 0 | 73 | 2202 | 0 | 152 | 326 | 21 | 91 | 230 | 0 |
| Heavy Vehicles（\％） | 1\％ | 2\％ | 1\％ | 2\％ | 4\％ | 4\％ | 1\％ | 1\％ | 1\％ | 3\％ | 3\％ | 2\％ |
| Turn Type | Prot | NA |  | Prot | NA |  | Prot | NA | Perm | Perm | NA |  |
| Protected Phases | 1 | 6 |  | 5 | 2 |  | 7 | 4 |  |  | 8 |  |
| Permitted Phases |  |  |  |  |  |  |  |  | 4 | 8 |  |  |
| Actuated Green，G（s） | 32.1 | 121.0 |  | 12.8 | 101.7 |  | 10.7 | 46.3 | 46.3 | 29.3 | 29.3 |  |
| Effective Green， g （s） | 32.1 | 121.0 |  | 12.8 | 101.7 |  | 10.7 | 46.3 | 46.3 | 29.3 | 29.3 |  |
| Actuated g／C Ratio | 0.16 | 0.60 |  | 0.06 | 0.51 |  | 0.05 | 0.23 | 0.23 | 0.15 | 0.15 |  |
| Clearance Time（s） | 6.8 | 6.8 |  | 6.8 | 6.8 |  | 6.3 | 6.3 | 6.3 | 6.3 | 6.3 |  |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  |
| Lane Grp Cap（vph） | 286 | 3053 |  | 113 | 2509 |  | 185 | 435 | 370 | 96 | 257 |  |
| v／s Ratio Prot | c0．14 | 0.47 |  | 0.04 | c0．45 |  | 0.04 | c0．17 |  |  | 0.13 |  |
| v／s Ratio Perm |  |  |  |  |  |  |  |  | 0.01 | c0．14 |  |  |
| v／c Ratio | 0.90 | 0.78 |  | 0.65 | 0.88 |  | 0.82 | 0.75 | 0.06 | 0.95 | 0.90 |  |
| Uniform Delay，d1 | 82.3 | 29.7 |  | 91.4 | 43.6 |  | 93.7 | 71.5 | 59.8 | 84.6 | 83.9 |  |
| Progression Factor | 1.45 | 0.24 |  | 1.06 | 0.89 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Incremental Delay，d2 | 21.0 | 1.5 |  | 10.4 | 4.1 |  | 24.5 | 6.9 | 0.1 | 74.1 | 30.3 |  |
| Delay（s） | 140.2 | 8.7 |  | 107.4 | 43.1 |  | 118.2 | 78.4 | 59.9 | 158.7 | 114.2 |  |
| Level of Service | F | A |  | F | D |  | F | E | E | F | F |  |
| Approach Delay（s） |  | 21.4 |  |  | 45.1 |  |  | 86.1 |  |  | 126.5 |  |
| Approach LOS |  | C |  |  | D |  |  | F |  |  | F |  |

Intersection Summary

| HCM 2000 Control Delay | 42.9 | HCM 2000 Level of Service | D |
| :--- | ---: | :--- | ---: |
| HCM 2000 Volume to Capacity ratio | 0.90 |  | 26.2 |
| Actuated Cycle Length（s） | 200.0 | Sum of lost time（s） | F |
| Intersection Capacity Utilization | $99.3 \%$ | ICU Level of Service |  |
| Analysis Period（min） | 15 |  |  |
| c Critical Lane Group |  |  |  |

HCM Signalized Intersection Capacity Analysis
3: Lee PI \& Hillsborough Ave


## HCM Signalized Intersection Capacity Analysis

3: Lee PI \& Hillsborough Ave

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }_{1}$ | 平个 |  | ${ }^{7}$ |  |  | 7 | F |  |  | 4 |  |
| Traffic Volume (vph) | 18 | 2198 | 10 | 81 | 2181 | 14 | 37 | 1 | 11 | 13 | 0 | 3 |
| Future Volume (vph) | 18 | 2198 | 10 | 81 | 2181 | 14 | 37 | 1 | 11 | 13 | 0 | 3 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 6.9 | 6.9 |  | 6.9 | 6.9 |  | 6.6 | 6.6 |  |  | 6.6 |  |
| Lane Util. Factor | 1.00 | 0.91 |  | 1.00 | 0.91 |  | 1.00 | 1.00 |  |  | 1.00 |  |
| Fit | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 0.86 |  |  | 0.98 |  |
| Flt Protected | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 |  |  | 0.96 |  |
| Satd. Flow (prot) | 1703 | 5082 |  | 1787 | 4984 |  | 1752 | 1623 |  |  | 1764 |  |
| Fit Permitted | 0.06 | 1.00 |  | 0.05 | 1.00 |  | 0.75 | 1.00 |  |  | 0.76 |  |
| Satd. Flow (perm) | 111 | 5082 |  | 103 | 4984 |  | 1377 | 1623 |  |  | 1387 |  |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Adj. Flow (vph) | 19 | 2290 | 10 | 84 | 2272 | 15 | 39 | 1 | 11 | 14 | 0 | 3 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 0 | 0 | 16 | 0 |
| Lane Group Flow (vph) | 19 | 2300 | 0 | 84 | 2287 | 0 | 39 | 2 | 0 | 0 | 1 | 0 |
| Heavy Vehicles (\%) | 6\% | 2\% | 1\% | 1\% | 4\% | 1\% | 3\% | 1\% | 1\% | 1\% | 1\% | 1\% |
| Turn Type | pm+pt | NA |  | pm+pt | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases | 1 | 6 |  | 5 | 2 |  |  | 4 |  |  | 8 |  |
| Permitted Phases | 6 |  |  | 2 |  |  | 4 |  |  | 8 |  |  |
| Actuated Green, G (s) | 164.1 | 160.5 |  | 175.1 | 166.0 |  | 10.0 | 10.0 |  |  | 10.0 |  |
| Effective Green, g (s) | 164.1 | 160.5 |  | 175.1 | 166.0 |  | 10.0 | 10.0 |  |  | 10.0 |  |
| Actuated g/C Ratio | 0.82 | 0.80 |  | 0.88 | 0.83 |  | 0.05 | 0.05 |  |  | 0.05 |  |
| Clearance Time (s) | 6.9 | 6.9 |  | 6.9 | 6.9 |  | 6.6 | 6.6 |  |  | 6.6 |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |  | 3.0 |  |
| Lane Grp Cap (vph) | 119 | 4078 |  | 166 | 4136 |  | 68 | 81 |  |  | 69 |  |
| v/s Ratio Prot | 0.00 | c0.45 |  | c0.02 | c0.46 |  |  | 0.00 |  |  |  |  |
| v/s Ratio Perm | 0.13 |  |  | 0.42 |  |  | c0.03 |  |  |  | 0.00 |  |
| v/c Ratio | 0.16 | 0.56 |  | 0.51 | 0.55 |  | 0.57 | 0.02 |  |  | 0.01 |  |
| Uniform Delay, d1 | 4.1 | 7.1 |  | 9.7 | 5.3 |  | 92.9 | 90.3 |  |  | 90.3 |  |
| Progression Factor | 0.13 | 0.08 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  |  | 1.00 |  |
| Incremental Delay, d2 | 0.4 | 0.4 |  | 2.4 | 0.5 |  | 11.2 | 0.1 |  |  | 0.1 |  |
| Delay (s) | 0.9 | 0.9 |  | 12.1 | 5.9 |  | 104.1 | 90.4 |  |  | 90.4 |  |
| Level of Service | A | A |  | B | A |  | F | F |  |  | F |  |
| Approach Delay (s) |  | 0.9 |  |  | 6.1 |  |  | 100.9 |  |  | 90.4 |  |
| Approach LOS |  | A |  |  | A |  |  | F |  |  | F |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 4.9 | HCM 2000 Level of Service | A |
| HCM 2000 Volume to Capacity ratio | 0.57 |  | 20.4 |
| Actuated Cycle Length (s) | 200.0 | Sum of lost time (s) | C |
| Intersection Capacity Utilization | $72.5 \%$ | ICU Level of Service |  |
| Analysis Period (min) | 15 |  |  |
| C Critical Lane Group |  |  |  |

Intersection: 1: Armenia Ave \& Hillsborough Ave

| Movement | EB | EB | EB | EB | EB | EB | WB | WB | WB | WB | WB | WB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | L | T | T | T | R | L | L | T | T | T | R |
| Maximum Queue (tt) | 208 | 458 | 606 | 545 | 512 | 250 | 205 | 355 | 770 | 800 | 844 | 102 |
| Average Queue (tt) | 106 | 208 | 401 | 363 | 316 | 126 | 98 | 213 | 495 | 534 | 563 | 28 |
| 95th Queue (tt) | 209 | 406 | 672 | 608 | 558 | 290 | 192 | 426 | 919 | 937 | 959 | 148 |
| Link Distance (ft) |  |  | 1273 | 1273 | 1273 |  |  |  | 2570 | 2570 | 2570 |  |
| Upstream Bik Time (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penally (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (ft) | 360 | 360 |  |  |  | 200 | 255 | 25 |  |  |  | 200 |
| Storage Blk Time (\%) |  | 0 | 14 |  | 19 |  |  | 0 | 21 |  | 28 |  |
| Queuing Penally (veh) |  | 0 | 22 |  | 34 |  |  | 2 | 44 |  | 16 |  |

Intersection: 1: Armenia Ave \& Hillsborough Ave

| Movement | NB | NB | NB | SB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | T | TR | L | T | TR |
| Maximum Queue (ft) | 209 | 399 | 342 | 289 | 591 | 539 |
| Average Queue (ft) | 171 | 244 | 218 | 238 | 452 | 398 |
| 95th Queue (ft) | 240 | 431 | 347 | 353 | 642 | 561 |
| Link Distance (ft) |  | 1293 | 1293 |  | 974 | 974 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |
| Storage Bay Dist (ft) | 160 |  |  | 240 |  |  |
| Storage Blk Time (\%) | 36 | 17 |  | 15 | 45 |  |
| Queuing Penalty (veh) | 51 | 30 |  | 44 | 100 |  |

Intersection: 1: Armenia Ave \& Hillsborough Ave

| Movement | EB | EB | EB | EB | EB | EB | WB | WB | WB | WB | WB | WB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | L | T | T | T | R | L | L | T | T | T | R |
| Maximum Queue (t) | 410 | 459 | 857 | 839 | 698 | 250 | 136 | 354 | 759 | 793 | 807 | 250 |
| Average Queue (f) | 378 | 427 | 637 | 567 | 428 | 125 | 52 | 122 | 513 | 548 | 569 | 141 |
| 95th Queue (t) | 441 | 505 | 1123 | 1002 | 718 | 303 | 118 | 318 | 826 | 846 | 877 | 328 |
| Link Distance ( t ) |  |  | 1273 | 1273 | 1273 |  |  |  | 2570 | 2570 | 2570 |  |
| Upstream BIk Time (\%) |  |  | 1 | 0 |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  | 0 | 0 |  |  |  |  |  |  |  |  |
| Storage Bay Dist (t) | 360 | 360 |  |  |  | 200 | 255 | 255 |  |  |  | 200 |
| Storage Blk Time (\%) | 21 | 42 | 15 |  | 26 |  |  |  | 33 |  | 43 |  |
| Queuing Penalty (veh) | 142 | 289 | 63 |  | 46 |  |  |  | 41 |  | 62 |  |

Intersection: 1: Armenia Ave \& Hillsborough Ave

| Movement | NB | NB | NB | SB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | T | TR | L | T | TR |
| Maximum Queue (ft) | 210 | 747 | 736 | 289 | 441 | 448 |
| Average Queue (ft) | 192 | 625 | 581 | 231 | 275 | 276 |
| 95th Queue (ft) | 237 | 814 | 763 | 326 | 486 | 459 |
| Link Distance (ft) |  | 1293 | 1293 |  | 974 | 974 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |
| Storage Bay Dist (ft) | 160 |  |  | 240 |  |  |
| Storage Blk Time (\%) | 47 | 56 |  | 33 | 11 |  |
| Queuing Penalty (veh) | 143 | 121 |  | 56 | 15 |  |

Intersection: 2: Rome Ave \& Hillsborough Ave

| Movement | EB | EB | EB | EB | WB | WB | WB | WB | NB | NB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | T | T | TR | L | T | T | TR | L | L | T | R |
| Maximum Queue $(\mathrm{ft})$ | 368 | 526 | 554 | 582 | 248 | 484 | 480 | 481 | 142 | 169 | 238 | 66 |
| Average Queue $(\mathrm{ft})$ | 154 | 306 | 341 | 363 | 139 | 367 | 370 | 382 | 85 | 127 | 143 | 40 |
| 95th Queue $(\mathrm{ft})$ | 344 | 603 | 641 | 687 | 268 | 556 | 552 | 537 | 167 | 186 | 250 | 74 |
| Link Distance $(\mathrm{ft})$ |  | 2570 | 2570 | 2570 |  | 1918 | 1918 | 1918 |  |  | 1381 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (ft) | 435 |  |  |  | 245 |  |  |  | 100 | 100 |  | 260 |
| Storage Blk Time (\%) |  | 3 |  |  | 1 | 26 |  |  | 8 | 46 | 30 |  |
| Queuing Penalty (veh) |  | 3 |  |  | 8 | 23 |  |  | 20 | 112 | 70 |  |

Intersection: 2: Rome Ave \& Hillsborough Ave

| Movement | SB | SB |
| :--- | ---: | ---: |
| Directions Served | L | TR |
| Maximum Queue (ft) | 109 | 733 |
| Average Queue (ft) | 83 | 604 |
| 95th Queue (ft) | 134 | 959 |
| Link Distance (ft) |  | 935 |
| Upstream Blk Time (\%) |  | 10 |
| Queuing Penalty (veh) |  | 0 |
| Storage Bay Dist (ft) | 60 |  |
| Storage Blk Time (\%) | 37 | 63 |
| Queuing Penalty (veh) | 126 | 86 |

Intersection: 2: Rome Ave \& Hillsborough Ave

| Movement | EB | E8 | EB | EB | WB | WB | WB | WB | NB | NB | NB | NB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | T | TR | L | T | T | TR | L | L | T | R |
| Maximum Queue ( ft ) | 314 | 258 | 277 | 308 | 218 | 378 | 418 | 437 | 25 | 89 | 1346 | 310 |
| Average Queue ( ft ) | 218 | 145 | 172 | 191 | 88 | 257 | 284 | 296 | 3 | 82 | 895 | 110 |
| 95th Queue (ft) | 299 | 285 | 311 | 332 | 216 | 398 | 445 | 474 | 20 | 91 | 1508 | 344 |
| Link Distance ( ft ) |  | 2570 | 2570 | 2570 |  | 1918 | 1918 | 1918 |  |  | 1381 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  | 16 |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  | 0 |  |
| Storage Bay Dist (ft) | 435 |  |  |  | 245 |  |  |  | 40 | 40 |  | 260 |
| Storage Blk Time (\%) |  |  |  |  |  | 11 |  |  | 0 | 91 | 31 |  |
| Queuing Penalty (veh) |  |  |  |  |  | 7 |  |  | 0 | 352 | 70 |  |

Intersection: 2: Rome Ave \& Hillsborough Ave

| Movement | SB | SB |
| :--- | ---: | ---: |
| Directions Served | L | TR |
| Maximum Queue (ft) | 109 | 498 |
| Average Queue (ft) | 79 | 369 |
| 95th Queue (ft) | 133 | 602 |
| Link Distance (ft) |  | 935 |
| Upstream Blk Time (\%) |  |  |
| Queuing Penalty (veh) |  |  |
| Storage Bay Dist (ft) | 60 |  |
| Storage Blk Time (\%) | 32 | 74 |
| Queuing Penalty (veh) | 72 | 63 |

Intersection: 3: Lee PI \& Hillsborough Ave

| Movement | EB | EB | EB | EB | WB | WB | WB | WB | NB | NB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | T | TR | L | T | T | TR | L | TR | LTR |
| Maximum Queue (ft) | 25 | 47 | 36 | 58 | 76 | 109 | 125 | 101 | 65 | 38 | 70 |
| Average Queue ( ft ) | 4 | 9 | 6 | 11 | 45 | 59 | 56 | 46 | 26 | 11 | 49 |
| 95th Queue ( tt ) | 19 | 39 | 29 | 46 | 82 | 128 | 135 | 116 | 67 | 39 | 81 |
| Link Distance ( ft ) |  | 1918 | 1918 | 1918 |  | 2494 | 2494 | 2494 |  | 542 | 372 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist ( ft ) | 200 |  |  |  | 375 |  |  |  | 200 |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |

Intersection: 3: Lee PI \& Hillsborough Ave

| Movement | EB | EB | EB | EB | WB | WB | WB | WB | NB | NB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | T | TR | L | T | T | TR | L | TR | LTR |
| Maximum Queue (t) | 30 | 77 | 94 | 79 | 91 | 120 | 152 | 128 | 94 | 37 | 42 |
| Average Queue (t) | 16 | 20 | 23 | 38 | 52 | 70 | 76 | 63 | 43 | 12 | 17 |
| 95th Queue (ft) | 36 | 65 | 82 | 84 | 98 | 139 | 156 | 137 | 89 | 38 | 44 |
| Link Distance (t) |  | 1918 | 1918 | 1918 |  | 2494 | 2494 | 2494 |  | 542 | 372 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (tt) <br> Storage Bik Time (\%) |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |

Roadway Cost Per Centerline Mile Revised August 2023

|  | Construction Cost From LRE | MOT* | Mobilization * | Subtotal | Scope Contingency $(25 \%)$ | Total Construction Cost | $\begin{array}{\|l} \text { PE Design } \\ (15 \%) \end{array}$ | CE (15\%) | Total Project Cost ${ }^{*}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rural Arterial |  |  |  |  |  |  |  |  |  |
| New Construction (2-Lane Roadway) with 5' Paved Shoulders | \$7,952,180 | \$795,218 | \$874,740 | \$9,622,138 | \$2,405,534 | \$12,027,672 | \$1,804,151 | \$1,804,151 | \$15,635,974 |
| New Construction (4-Lane Roadway) with 5' Paved Shoulders | \$12,976,186 | \$1,297,619 | \$1,427,380 | \$15,701,185 | \$3,925,296; | \$19,626,481 | \$2,943,972 | \$2,943,972 | \$25,514,426 |
| New Construction (6-Lane Roadway) with 5' Paved Shoulders | \$16,565,915 | \$1,656,592 | \$1,822,251 | \$20,044,757 | \$5,011,189 | \$25,055,947 | \$3,758,392 | \$3,758,392 | \$32,572,731 |
| Milling and Resurfacing (4-Lane Roadway) with 5' Paved Shoulders | \$1,953,521 | \$195,352 | \$214,887 | \$2,363,760 | \$590,940 | \$2,954,701 | \$443,205 | \$443,205 | \$3,841,111 |
| Milling and Resurfacing (6-Lane Roadway) with 5' Paved Shoulders | \$2,768,817 | \$276,882 | \$304,570 | \$3,350,268 | \$837,567' | \$4,187,835 | \$628,175 | \$628,175 | \$5,444,186 |
| Add Lanes (2 to 4 Lanes) with 5' Paved Shoulders (Includes milling and resurfacing of existing pavement) | \$9,356,824 | \$935,682 | \$1,029,251 | \$11,321,757 | \$2,830,439 | \$14,152,196 | \$2,122,829 | \$2,122,829 | \$18,397,855 |
| Add Lanes (4 to 6 Lanes) with 5' Paved Shoulders (Includes milling and resurfacing of existing pavement) | \$9,768,149 | \$976,815 | \$1,074,496 | \$11,819,461 | \$2,954,865 | \$14,774,326 | \$2,216,149 | \$2,216,149 | \$19,206,623 |
| Add Lanes (4 to 8 Lanes) with 5' Paved Shoulders (Includes milling and resurfacing of existing pavement) | \$13,673,462 | \$1,367,346 | \$1,504,081 | \$16,544,889 | \$4,136,222 | \$20,681,111 | \$3,102,167 | \$3,102,167 | \$26,885,444 |
| Add Lanes (6 to 8 Lanes) with 5' Paved Shoulders (Includes milling and resurfacing of existing pavement) | \$12,316,312 | \$1,231,631 | \$1,354,794 | \$14,902,738 | \$3,725,684 | \$18,628,422 | \$2,794,263 | \$2,794,263 | \$24,216,949 |
| Add 1 Through Lane on Inside (To Existing) with 5' Paved Shoulders | \$2,467,321 | \$246,732 | \$271,405 | \$2,985,458 | \$746,364 | \$3,731,822 | \$559,773 | \$559,773 | \$4,851,369 |
| Add 1 Through Lane on Outside (To Existing) with 5' Paved Shoulders | \$3,738,718 | \$373,872 | \$411,259 | \$4,523,849 | \$1,130,962 | \$5,654,811 | \$848,222 | \$848,222 | \$7,351,254 |
| Add $300^{\prime}$ Exclusive Left Turn Lane | \$116,112 | \$17,417 | \$20,029 | \$153,558 | \$38,389 | \$191,947 | \$28,792 | \$28,792 | \$249,531 |
| Add 300' Exclusive Right Turn Lane | \$301,916 | \$45,287 | \$52,081 | \$399,284 | \$99,821 | \$499,105 | \$74,866 | \$74,866 | \$648,836 |
| Urban Arterial |  |  |  |  |  |  |  |  |  |
| New Construction (2-Lane Roadway) with 5' Sidewalk, and Curb \& Gutter | \$12,384,197 | \$1,238,420 | \$1,362,262 | \$14,984,879 | \$3,746,220 | \$18,731,098 | \$2,809,665 | \$2,809,665 | \$24,350,428 |
| New Construction (4-Lane Roadway) with 5' Sidewalk, and Curb \& Gutter | \$17,308,028 | \$1,730,803 | \$1,903,883 | \$20,942,714 | \$5,235,678 | \$26,178,392 | \$3,926,759 | \$3,926,759 | \$34,031,910 |
| New Construction (6-Lane Roadway) with 5' Sidewalk, and Curb \& Gutter | \$21,044,989 | \$2,104,499 | \$2,314,949 | \$25,464,437 | \$6,366,109 | \$31,830,546 | \$4,774,582 | \$4,774,582 | \$41,379,710 |
| Milling and Resurfacing (4-Lane Roadway) with 5' Sidewalk, and Curb \& Gutter | \$2,047,760 | \$204,776 | \$225,254 | \$2,477,790 | \$619,447 | \$3,097,237 | \$464,586 | \$464,586 | \$4,026,408 |
| Milling and Resurfacing (6-Lane Roadway) with 5' Sidewalk, and Curb \& Gutter | \$2,899,664. | \$289,966 | \$318,983 | \$3,508,593 | \$877,148 | \$4,385,741 | \$657,861 | \$657,861 | \$5,701,464 |
| Add Lanes (2 to 4 Lanes) with 5' Sidewalk, and Curb \& Gutter (Inciudes milling and resurfacing existing pavement) | \$12,120,747 | \$1,212,075 | \$1,333,282 | \$14,666,104 | \$3,666,526 | \$18,332,630 | \$2,749,895 | \$2,749,895 | \$23,832,419 |
| Add Lanes (4 to 6 Lanes) with 5' Sidewalk, and Curb \& Gutter (Includes milling and resurfacing existing pavement) | \$13,102,423 | \$1,310,242 | \$1,441,267 | \$15,853,932 | \$3,963,483 | \$19,817,415 | \$2,972,612 | \$2,972,612 | \$25,762,640 |
| Add Lanes (4 to 8 Lanes) with 5 ' Sidewalk, and Curb \& Gutter (Includes milling and resurfacing existing pavement) | \$18,056,515, | \$1,805,651 | \$1,986,217 | \$21,848,383 | \$5,462,096 | \$27,310,478 | \$4,096,572 | \$4,096,572 | \$35,503,622 |
| Add Lanes (6 to 8 Lanes) with 5' Sidewalk, and Curb \& Gutter (Includes milling and resurfacing existing pavement) | \$15,304,417 | \$1,530,442 | \$1,683,486 | \$18,518,345 | \$4,629,586 | \$23,147,931 | \$3,472,190 | \$3,472,190 | \$30,092,310 |
| Add 1 Through Lane on Inside (To Existing) with 5' Sidewalk, and Curb \& Gutter | \$2,249,957 | \$224,996 | \$247,495 | \$2,722,449 | \$680,612 | \$3,403,061 | \$510,459 | \$510,459 | \$4,423,979 |
| Add 1 Through Lane on Outside (To Existing) with 5' Sidewalk, and Curb \& Gutter | \$6,415,889 | \$641,589 | \$705,748 | \$7,763,226 | \$1,940,806 | \$9,704,032 | \$1,455,605 | \$1,455,605 | \$12,615,241 |
| Add 300' Exclusive Left Turn Lane | \$155,949 | \$23,392 | \$26,901 | \$206,242 | \$51,561 | \$257,803 | \$38,670 | \$38,670 | \$335,144 |
| Add 300' Exclusive Right Turn Lane | \$360,812 | \$54,122 | \$62,240 | \$477,174 | \$119,294 | \$596,468 | \$89,470 | \$89,470 | \$775,408 |

** Total cost shown is derived from a standard typical section. Costs will need to be adjusted to account for signals, bridges, or any additional item not deemed typical.
2. These figures exclude costs for intersectionsinterchanges, improvements to cross streets, bridges over 20', right-of-way, landscaping, ITS, and traffic signals. 3. The figures are based on market costs for Hillsborough County.
4. Cosis shown are present day costs.

FDOT DESIGN MANUAL EXHIBIT 212-1
MEDIAN TURN LANES MINIMUM DECELERATION LENGTHS


| MEDIAN TURN LANES |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Design } \\ & \text { Speed } \\ & \text { (mph) } \end{aligned}$ | Entry <br> Speed <br> (mph) | $\begin{gathered} \text { Clearance } \\ \text { Distance } \\ L_{1}\left(f \mathrm{ft}^{2}\right) \end{gathered}$ | URBAN CONDITIONS |  |  | RURAL CONDITIONS |  |  |
|  |  |  | Brake To Stop Distance $L_{2}$ (ft.) |  | Clearance Distance $L,(f t$. | Brake To 5too Distance $L_{2}$ (ft.) |  | $\begin{gathered} \text { Clearance } \\ \text { Distance } \\ L_{J}(f t .) \end{gathered}$ |
| 35 | 25 | 70 | 75 | 145 | 110 | - | - | - |
| 40 | 30 | 80 | 75 | 155 | 120 | - | - | - |
| 45 | 35 | 85 | 100 | 185 | 135 | - | - | - |
| 50 | 40/44 | 105 | 135 | 240 | 160 | 185 | 290 | 160 |
| 55 | 48 | 125 | - | - | - | 225 | 350 | 195 |
| 60 | 52 | 145 | - | - | - | 260 | 405 | 230 |
| 65 | 55 | 170 | - | - | - | 290 | 460 | 270 |


[^0]:    (1) Source: FDOT Roadway Cost Per Centerline Mile, Revised August, 2023. Hillsborough Ave and Armenia Ave
    $\mathrm{EBR}=540(\mathrm{a}) / 300 \times \$ 775,408=\$ 1,395,734$
    Hillsborough Ave and Rome Ave
    NBL $=345(\mathrm{a}) / 300 \times \$ 335,144=\$ 385,416$
    Hillsborough Ave and Lee Place
    (a) Based on queue storage length plus deceleration length
    2) ROW costs $125 \%$ of construction costs.
    (3) \% LOS D Consumed-See Table A1 in the Appendix.

[^1]:    Notes
    ＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．

[^2]:    Notes
    ＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．

